

AD-A009 157

A REVISED COMPUTER PROGRAM FOR AXIAL COMPRESSOR DESIGN.
VOLUME II. PROGRAM LISTING AND PROGRAM USE EXAMPLE

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19. KEY WORDS (Continue on reverse side if necessary and identify by block number) axial compressor test data analysis computer program <div style="text-align: center;">Reproduced by NATIONAL TECHNICAL INFORMATION SERVICE U.S. Department of Commerce Springfield, VA 22151</div>		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) A revised computer program for the design of axial compressors is presented. It comprises three principal sections, two alternative means of determining blade geometry and an aerodynamic computation for the flow through the compressor. One method of determining blade geometry uses various analytic meanlines for the blade sections, and leads to the aerodynamic analysis of the flow through specified blading. The other		

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method consists of creating arbitrary blade sections to follow the flow directions previously determined in an aerodynamic design calculation. The aerodynamic design section incorporates a loss calculation routine that may be used to estimate the design point performance of the compressor. One, two, or all three sections may be used in any one run of the program. This second volume of two describing the program shows the FORTRAN program listing and an example of the use of the program.

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PREFACE

The work described in this Final Report was performed by the University of Dayton Research Institute, 300 College Park Avenue, Dayton, Ohio 45469, under Air Force Contract F33615-74-C-4030 during the period October 1973 to October 1974. It was a portion of Project 7065, Task 04 of the Aerospace Research Laboratories, and Project 3066 of the Aero Propulsion Laboratory. Technical Monitors for the Air Force were Dr. A. J. Wennerstrom, ARL/LF, and Mr. M. A. Stibich, AFAPL/TBC, both at Wright-Patterson Air Force Base, Ohio 45433. This report was initially identified as UDRI-TR-74-47 by the University of Dayton.

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SECTION I

FORTRAN PROGRAM LISTING

The following pages show the FORTRAN program listings. Each program or subprogram is begun on a new page, except that the fluid properties package, Subroutine UDG1 through Function UDG9, has been listed as a single unit.

[illegible]

[illegible]

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110 254 IF(NSPLIT,E0.1)GO TO 170
111 LI=NSPEC(1)
112 XX1(1)=0.0
113 DO 110 K=2,L1
114 XX1(K)=XX1(K-1)+SQRT((RSTN(K)-RSTN(K-1))**2+(XSTN(K)-XSTN(K-1))**2)
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200 DO 200 K=1,11
   XX2(K)=FLOCAT(K-1)*J,1
   CALL UD0301(XX1,XSTN(L1),L2,XX2,XX3,X1,11,0,0)
   CALL UD0301(XX1,RSTN(L1),L2,XX2,XX4,X1,11,0,0)
   GO 230 K=2,11
   XX1(K)=XX1(K-1)+JURI((XX3(K)-XX3(K-1))*2+(XX4(K)-XX4(K-1))*2)
   GAMMA(K-1)=(XX4(K)+XX4(K-1))*0.5
   XX3(K-1)=(XX1(K)+XX1(K-1))*0.5
   IF(I-0.1,0.0,1.0,0.15)GO TO 234
   L3=ISI(I+1)
   L4=ISI(I-1)
   L5=L1
   XX2(1)=(ATAN2(PSTN(L3)-RSTN(L5),XSTN(L3)-XSTN(L5))+ATAN2(RSTN(L5)-
1 RSTN(L4),XSTN(L5)-XSTN(L4)))*0.5
   L3=L3+NSPEC(I+1)-1
   L4=L4+NSPEC(I-1)-1
   L5=L3+L2-1
   XX2(2)=(ATAN2(RSTN(L3)-RSTN(L5),XSTN(L3)-XSTN(L5))+ATAN2(FSTN(L5)-
1 RSTN(L4),XSTN(L3)-XSTN(L4)))*J.5
   GO TO 235
   IF(I-0,NS)GO TO 236
   L3=ISI(2)
   XX2(1)=ATAN2(PSTN(L3)-RSTN(1),XSTN(L3)-XSTN(1))
   L4=NSPEC(1)
   L3=L3+NSPEC(2)-1
   XX2(2)=ATAN2(PSTN(L3)-RSTN(L4),XSTN(L3)-XSTN(L4))
   GO TO 238
   L4=ISI(I-1)
   XX2(1)=ATAN2(PSTN(L1)-RSTN(L4),XSTN(L1)-XSTN(L4))
   L3=L4+NSPEC(I-1)-1
   L3=L4+L2-1
   XX2(2)=ATAN2(PSTN(L3)-RSTN(L4),XSTN(L3)-XSTN(L4))
   XI(1)=0.0
   XI(2)=XI(1)
   CALL UD0301(XI,XX2,2,XX3,PHI,X1,10,1,0)
   CALL UD0301(RSTN(L1),XSTN(L1),L2,GAMA,X1,GAMA,10,0,1)
   XX3(1)=0.0
   XI(1)=0.0
   DO 240 K=2,11
   XX3(K)=XX3(K-1)+COS(PHI(K-1)+ATAN(GAMA(K-1)))*(XX4(K)+XX4(K-1))*(X
1 X1(K)-X1(K-1))
   XI=1.0/X3(11)
   DO 244 K=2,11
   XX3(K)=XX3(K)*X1
   CALL UD0301(XX3,XX1,11,DELF,XL(1,I),X1,NSIRMS,1,0)
   XI=VV(L2)/XX1(11)
   DO 246 J=2,NSIRMS
   XL(J,I)=XL(J,I)*X1
   CALL UD0301(VV,XSTN(L1),L2,XL(1,I),X1,NSIRMS,0,0)
   CALL UD0301(VV,XSTN(L1),L2,XL(1,I),X1,NSIRMS,0,0)
   IF(ICAS-0.07,1.0)GO TO 270

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260      X1=X(IMID,2)-X(IMID,1))*2+(R(IMID,2)-R(IMID,1))*2
      ORDM2(1)=(R(NSIRMS,1)-R(1,1))*2+(X(NSIRMS,1)-X(1,1))*2/X1
      L1=NSINS-1
      DO 260 I=2,L1
      X2=X(IMID,I+1)-X(IMID,I))*2+(R(IMID,I+1)-R(IMID,I))*2
      X3=X2
      IF(X1.LT.X3)X3=X1
      ORDM2(I)=(R(NSIRMS,I)-R(1,I))*2+(X(NSIRMS,I)-X(1,I))*2/X3
      X1=X2
      ORDM2(NSINS)=(R(NSIRMS,NSINS)-R(1,NSINS))*2+(X(NSIRMS,NSINS)-X(1,
1,NSINS))*2/X2
      DO 280 I=1,NSINS
      VMOL(I)=WBLOCK(I)
      IPASS=1
      IF(IPASS.GT.1.OR.ICASE.GT.1).AND.NDATA(1).EQ.1)GO TO 400
      L1=NDIMEN(1)+1
      GO TO(300,320,340,360),L1
      DO 310 J=1,NSIRMS
      XX1(J)=R(J,1)
      GO TO 320
      DO 330 J=1,NSIRMS
      XX1(J)=R(J,1)/R(NSIRMS,1)
      GO TO 340
      DO 350 J=1,NSIRMS
      XX1(J)=XL(J,1)
      GO TO 360
      DO 370 J=1,NSIRMS
      XX1(J)=XL(J,1)/XL(NSIRMS,1)
      L1=NDATA(1)
      L2=NDATA(1)
      CALL UD0301(J,ATA1,L2,XX1,S,X1,NSIRMS,L1,0)
      CALL UD0301(J,ATA2,L2,XX1,H,X1,NSIRMS,L1,0)
      CALL UD0301(J,ATA3,L2,XX1,TBETA,X1,NSIRMS,L1,0)
      GO 390 J=1,NSIRMS
      H(J,1)=UDG6(S(J,1),H(J,1))
      TBETA(J,1)=UDG3(S(J,1),H(J,1))
      IF(IPASS.GT.1).OR.ICASE.GT.1)GO TO 420
      X1=FLOW(1)/(UDG5(H,S)*PI*(F(NSIRMS,1)+X(1,1))*XL(NSIRMS,1))*5CLFAC
      X1**2
      DO 410 J=1,NSIRMS
      VM(J,1)=X1
      IF(ISTAG.EQ.1)VM(1,1)=0.0
      IF(FAIL=0)
      IFFAIL=0
      IFFAIL=0
      GO 430 J=1,NSIRMS
      VMOL(J)=VM(J,1)
      GO TO 500

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440 IF (IPASS.GT.1) GO TO 450
450 GO 450 J=1,NSTRMS
460 VM(J,I)=VM(J,I-1)
470 IF (I-1.EQ.0) ISTAG=VM(1,I)=0.0
480 ILOSS=1
490 DO 464 J=1,NSTRMS
500 VMOLD(J)=VM(J,I)
510 DO 474 J=1,NSTRMS
520 VMKEEP(J)=VM(J,I-1)
530 HXKEEP(J)=H(J,I-1)
540 XI=H(IMID,I-1)-(VM(IMID,I-1)*2+VM(IMID,I-1)**2)/(2.0*G*EJ)
550 PSMID=UUG4,X1,H*Y1,X1=H*Y1
560 IF (X1.LT.0) X1=0
570 IF (X1.GT.1) X1=1
580 IF (X1.EQ.0) X1=0.5
590 IF (X1.EQ.1) X1=1
600 IF (X1.EQ.0.5) X1=0.5
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990 IF (X1.EQ.0.5) X1=0.5
1000 IF (X1.EQ.0.5) X1=0.5

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540 ILOSS=ILOSS+1
540 J=1,NSTRM3
540 VMLOLD(J)=VM(J,I)
540 GO TO 570
550 IF(IPASS,LE,NFORCE)GO TO 570
550 IF(LNCT+1,LE,NPAGE)GO TO 570
560 WRITE(LOG2,560)
560 FORMAT(1H1)
570 LNCT=1
570 LNCT=LNCT+1
570 X1=VM(1,I)/VMLOLD(1)
570 X2=VM(IMID,I)/VMLOLD(IMID)
570 X3=VM(NSTRM3,I)/VMLOLD(NSTRM3)
580 WRITE(LOG2,580)IPASS,I,X1,X2,X3
580 FORMAT(5X,4HPASS,I3,9H STATI ON,I3,66H VM PROFILE NOT CONVERGED W
580 IFTH LOSS RECALC VM NEW/VM PREV HUB=F9.6,5H MID=F9.6,7H CASE
590 IF(F9.6)
590 IF(NRL.EQ.1.AND.(IFAILD.EQ.0.OR.IPASS.LE.NFORCE))CALL UD0310
600 DO 600 J=1,NSTRM3
600 X1(J)=X(J,I)
600 IF(I.EQ.1)GO TO 600
600 IF(ABS(VM(J,I)/VMLOLD(J))-1.0).GT.TOLNCE)IVFAIL=IVFAIL+1
600 IF(ABS(DELW(J))-DELW(J)).GT.TOLNCE)IFFAIL=IFFAIL+1
600 CONTINUE
600 IF(NMAX.EQ.1.OR.(IPASS.EQ.1.AND.NREAD.EQ.1))GO TO 624
600 IF(FM2
600 IF(X1,LT,1.0-XMMAX)X1=1.0-XMMAX
600 X2=1.0
600 IF(I.EQ.1.09,NWORK(I),GE,5)X2=1.0+TBETA(IMID,I)**2
600 X1=1.0/(1.0+X1*DRU+2(I)/(RCONST*X2))
600 L3=NSTRM3-2
600 CALL UD0301(J,DELW,XL(1,I),NSTRMS,DELF(2),XX1(2),X1,L3,1,0)
600 XX=XL(IMID,I)
600 DO 610 J=2,IFUB
600 XL(J,I)=XL(J,I)+X1*...X1(J)-XL(J,I)
600 IF(I,PA
600 IF(L1,LE,59)GO TO 618
600 L1=59
600 DO 618 K=1,59
600 DELTAR(K,I)=DELTAR(K+1,I)
600 DELTAR(L1,I)=XL(IMID,I)-XX
600 L1=IS1(I)
600 L2=NSPEC(I)
600 XX1(1)=0.0
600 DO 620 K=2,L2
600 KK=L1-1+K
600 XX1(K)=XX1(K-1)+SORT((XSTN(KK)-XSTN(KK-1))*2+(RSTN(KK)-RSTN(KK-1))
600 )+2)
600 CALL UD0301(XX1,RSTN(L1),L2,XL(2,I),R(2,I),X1,L3,1,0)

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[illegible]


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SUBROUTINE UDJ31(XDATA,YDATA,NDATA,XIN,YOUT,SLOPE,NXY,NTYPE,NWOT)
REAL M
DIMENSION XDATA(1),YDATA(1),XIN(1),YOUT(1),SLOPE(1),A(21),B(21),D(
121),M(21)
IF(NTYPE.EQ.1.0).NDATA.LT.3IGJ TO 210
A(1)=1.0
B(1)=0.0
C(1)=0.0
V=NDATA-1
DO 110 I=2,N
A(I)=(XDATA(I+1)-XDATA(I-1))/3.0-(XDATA(I)-XDATA(I-1))*B(I-1)/(C.0
1+A(I-1))
B(I)=(XDATA(I+1)-XDATA(I))/6.0
C(I)=(YDATA(I+1)-YDATA(I))/(XDATA(I+1)-XDATA(I))-YDATA(I)-YDATA(I
1-1))/(XDATA(I)-XDATA(I-1))-(XDATA(I)-XDATA(I-1))*C(I-1)/(6.0*A(I-1
2))
A(NDATA)=0.0
B(NDATA)=1.0
C(NDATA)=0.0
M(NDATA)=A(N)*A(N)/A(NDATA)*3(N)-A(N)*B(NDATA)
DO 120 II=2,NDATA
Y(II)=(C(II)-C(II+1))/A(II)
Y(NDATA+1)=Y(II)
ASSIGN 130 TO IY
IF(NWOT.EQ.1)ASSIGN 160 TO IY
ASSIGN 150 TO ISLOPE
IF(NWOT.EQ.0)ASSIGN 200 TO ISLOPE
J=2
DO 200 I=1,NXY
IF(XIN(I).LT.XDATA(1))GO TO 170
IF(XIN(I).GT.XDATA(NDATA))GO TO 180
IF(XIN(I).LE.XDATA(J))GO TO 140
J=J+1
GO TO 130
EX=XDATA(J)-XDATA(J-1)
GO TO IY(150,150)
YOUT(I)=M(J-1)/(6.0*EX)*(XDATA(J)-XIN(I))+3*M(J)/(6.0*EX)*(XIN(I)
1-XDATA(J-1))+3*(XDATA(J)-XIN(I))*YDATA(J-1)/EX-M(J-1)/6.0*EX)
2 IN(I)-XDATA(J-1))*(YDATA(J)/EX-M(J)/6.0*EX)
GO TO ISLOPE(150,200)
SLOPE(I)=-M(J-1)*(XDATA(J)-XIN(I))*2/2.0+M(J)*(XIN(I)-XDATA(J-1)
1)*2/2.0+YDATA(J)-YDATA(J-1)/EX-(M(J)-M(J-1))/6.0*EX
GO TO 200
JP=1
JP=2
GO TO 140
JP=NDATA
JP=N
YPRIME=(YDATA(KP)-YDATA(JP))/(XDATA(KP)-XDATA(JP))-M(KP)/6.0*(XDATA
1A(KP)-XDATA(JP))

```

```

200 IF (NWOT.NE.0) YOUT(I)=YDATA(JP)+(XIN(I)-XDATA(JP))*YPRIME
210 CONTINUE
220 RETURN
230 IF (NDATA.NE.1) GO TO 230
240 I=1,NXY
250 YOUT(I)=YDATA(1)
260 RETURN
270 IF (NWOT.EQ.1) GO TO 254
280 J=2
290 I=1,NXY
300 IF (XIN(I).LE.XDATA(J).OR.J.EQ.NDATA) GO TO 250
310 J=J+1
320 GO TO 240
330 YOUT(I)=YDATA(J-1)+(YDATA(J)-YDATA(J-1))/(XDATA(J)-XDATA(J-1))*(XIN(I)-XDATA(J-1))+YPRIME
340 IN(I)=XDATA(J-1)
350 IF (NWOT.NE.2) RETURN
360 YPRIME=(YDATA(2)-YDATA(1))/(XDATA(2)-XDATA(1))
370 I=1,NXY
380 SLOPE(I)=YPRIME
390 RETURN
400 END

```



```

310  FORMAT(2X,/,13X,MODEL,8X,SHDELTA,/,/(13X,F9.4,F12.4))
320  CONTINUE
330  CALL U00303(LNCT,5+NSTNS)
340  GR=ADU(LOG1,330)(WBLOCK(I),BBLOCK(I),FOIST(I),I=1,NSTNS)
350  WRITE(LOG2,340)(I,WBLOCK(I),BBLOCK(I),BDIST(I),I=1,NSTNS)
360  WFORMAT(2X,/,13X,30HBLOCKAGE FACTOR SPECIFICATION,/,10X,66HSTATION
370  WFORMAT(2X,/,13X,30HBLOCKAGE FACTOR SPECIFICATION WAKE DISTRIBUTION FACTOR,/,10X,66HSTATION
380  WFORMAT(2X,/,13X,30HBLOCKAGE FACTOR SPECIFICATION WAKE DISTRIBUTION FACTOR,/,10X,66HSTATION
390  WFORMAT(2X,/,13X,30HBLOCKAGE FACTOR SPECIFICATION WAKE DISTRIBUTION FACTOR,/,10X,66HSTATION
400  WFORMAT(2X,/,13X,30HBLOCKAGE FACTOR SPECIFICATION WAKE DISTRIBUTION FACTOR,/,10X,66HSTATION
410  WFORMAT(2X,/,13X,30HBLOCKAGE FACTOR SPECIFICATION WAKE DISTRIBUTION FACTOR,/,10X,66HSTATION
420  WFORMAT(2X,/,13X,30HBLOCKAGE FACTOR SPECIFICATION WAKE DISTRIBUTION FACTOR,/,10X,66HSTATION
430  WFORMAT(2X,/,13X,30HBLOCKAGE FACTOR SPECIFICATION WAKE DISTRIBUTION FACTOR,/,10X,66HSTATION
440  WFORMAT(2X,/,13X,30HBLOCKAGE FACTOR SPECIFICATION WAKE DISTRIBUTION FACTOR,/,10X,66HSTATION
450  WFORMAT(2X,/,13X,30HBLOCKAGE FACTOR SPECIFICATION WAKE DISTRIBUTION FACTOR,/,10X,66HSTATION
460  WFORMAT(2X,/,13X,30HBLOCKAGE FACTOR SPECIFICATION WAKE DISTRIBUTION FACTOR,/,10X,66HSTATION

```

```

480 IF (NSTRMS.GT.16) L1=8
470 CALL UDU303(LNCT,L1)
WRITE(LUG2,470)
L1=NSTRMS
IF (NSTRMS.GT.15) L1=15
WRITE(LUG2,480) (J,J=1,L1)
FORMAT(2X,/,10X,10HSTREAMLINE,I5,14I7)
FORMAT(2X,/,10X,70HPROPORTIONS OF TOTAL FLOW BETWEEN HUB AND EACH
1 STREAMLINE ARE TO 3F AS FOLLOWS)
WRITE(LUG2,490) (DEL(J),J=1,L1)
FORMAT(10X,4HFLOW,7X,15F7.4)
IF (NSTRMS.LE.15) GO TO 500
L1=L1+1
WRITE(LUG2,490) (J,J=L1,NSTRMS)
WRITE(LUG2,490) (DEL(J),J=L1,NSTRMS)
IF (NPLAU.EQ.0) GO TO 570
READ(LUG1,510) ((R(J,I),X(J,I),XL(J,I),II(J,I),JJ(J,I),J=1,NSTRMS),
1 I=1,NSTRMS)
FORMAT(3F12,3,2I3)
CALL UDU303(LNCT,5+NSTRMS)
WRITE(LUG2,520)
FORMAT(2X,/,10X,32HESTIMATED STREAMLINE COORDINATES)
DO 530 I=1,NSTRMS
IF (I.GT.1) CALL UDU303(LNCT,3+NSTRMS)
WRITE(LUG2,540) (I,J,2(J,I),X(J,I),XL(J,I),II(J,I),JJ(J,I),J=1,NSTR
1 MS)
FORMAT(2X,/,10X,79HSTATION STREAMLINE RADIUS AXIAL COORDINATE
1 L-COORDINATE I J,/, (3X,2I11,F14.4,F12.4,F16.4,I17
2 I5))
GO TO 570
WRITE(LUG2,550)
FORMAT(1H1,10X,33HJOB STOPPED - TOO MUCH INPUT DATA)
STOP
RETURN
END

```



```

SUBROUTINE UD0329(H,S,VW,R1,R2,X1,X2,VM,EPS,SOLFAC,G,EJ,HMIN,VMIN,  

1$SMID,NSTRMS,LOG2,LNCF,IFAIL)  

DIMENSION H(21),S(1),VW(1),R1(1),R2(1),X1(1),X2(1),VM(1)  

1(20),DELTA(20),PSUP(21),VZON(21),PSDI(21),HUP(21),VMUP(21),  

21),VWDN(21),HJN(21),XX1(21),XX2(21),R(21)  

DO 80 J=1,NSTRMS  

P(J)=(R1(J)+R2(J))*0.5  

G1=P(NSTRMS)-P(1)  

G2=VM(1)  

DO 90 J=2,NSTRMS  

IF(P(J)-P(J-1).LT.1)Q1=R(J)-R(J-1)  

IF(VM(J)).LT.1)Q2=VM(J)  

CONTRINU.  

DELTA(Q2)*Q1**2/(EPS*SOLFAC)*0.25  

G1=(X2(1)+X2(NSTRMS)-X1(1)-X1(NSTRMS))*0.5  

ISTEP=Q1/DELTA+1.0  

DELTA=Q1/FLOR(ISTEP)  

VM2=VMIN*2  

ITUB=NSTRMS-1  

DO 110 J=1,NSTRMS  

PSUP(J)=PMI  

HUP(J)=H(J)  

VMUP(J)=VW(J)  

DO 120 J=1,ITUB  

RMID(J)=(R(J)+R(J+1))*0.5  

DELTA(J)=P(J+1)-P(J)  

IFAIL=0  

KSTEP=1  

CALL UD0329(VWUP,R,XX2,NSTRMS)  

DO 150 J=1,NSTRMS  

VMFUN(J)=EPS/J*(X2(J)-VMUP(J)/R(J))*SOLFAC  

IF(KSTEP.GT.1)GO TO 240  

JSTEP=1  

J1=IMIU  

J2=J1+JSTEP  

JJ=J1  

IF(JSTEP.EQ.-1)JJ=J2  

G1=((VMUP(J1)+VMUP(J2))*0.5)**2/RMID(JJ)  

G1=DELTA(JJ)*G1*FLUAT(JSTEP)  

X3=((SUP(J1)+SUP(J2))*0.5  

X=1  

G2=UDG2(X3,(PSUP(J1)+PSUP(J2))*0.5)  

IF(G2.GE.HMIN)GO TO 210  

IFAIL=1  

GO TO 3JU  

G2=UDG5(Q2,X3)/G  

X+=PSUP(J2)

```

```

PSUP(J2)=PSUP(J1)+J1*Q2
IF(ABS(X4/PSUP(J2)-1.0).LE.1.0E-5)GO TO 220
K=X+1
IF(K.LE.10)GO TO 200
IFAIL=2
GO TO 600
IF(J2.EG.1)GO TO 240
IF(J2.CG.NC1RMS)GO TO 230
J1=J2
GO TO 190
JSTEP=-1
J1=IMID
GO TO 190
DO 260 J=1,NSTRMS
  HSUP(J)=UDG2(SUP(J),PSUP(J))
  IF(HSUP(J).GE.HMIN)GO TO 250
  IFAIL=3
  GO TO 600
Q1=2.0*G*EJ*(HUP(J)-HSUP(J))-VHUP(J)**2
IF(Q1.GE.VM2)GO TO 250
IFAIL=4
GO TO 600
VZUP(J)=SORT(G1)
FLOW=0.0
DO 270 J=1,ITUB
  FLOW=FLOW+(R(J+1)**2-R(J)**2)*(VZUP(J)+VZUP(J+1))*UDG5((HSUP(J)+HSUP(J+1))*G.5,(SUP(J)+SUP(J+1))*J.5)
  CALL UD0324(HSUP,R,XX2,NSTRMS)
  DO 300 J=1,NSTRMS
    HON(J)=HUP(J)+DELZ/VZUP(J)*FPS/R(J)*XX2(J)*SCLFAC
  DO 310 J=1,NSTRMS
    VHON(J)=VHUP(J)+DELZ/VZUP(J)*VHFUN(J)
  CALL UD0324(VZUP,R,V7FUN,NSTRMS)
  DO 330 J=1,NSTRMS
    VZFUN(J)=DELZ*EPS*SCLFAC*VZFUN(J)/R(J)
  PSON(J)=SUP(J)
  PSUN(J)=PSUP(J)
  KK=1
  J1=IMID
  JSTEP=1
  J2=J1+JSTEP
  JJ=J1
  IF(JSTEP.EQ.-1)JJ=J2
  Q1=((VHON(J1)+VHON(J2))*0.5)**2/RMID(JJ)
  Q1=DELZ(JJ)*J1*FLOAT(JSTEP)
  X3=(SON(J1)+SON(J2))*0.5
  KK=1
  Q2=UDG2(X3,(PSON(J1)+PSON(J2))*0.5)
  IF(Q2.GE.HMIN)GO TO 370
  IFAIL=5

```

```

370      GO TO 410
      Q2=UDG5(Q2,X3)/G
      X4=PSUN(J2)
      PSUN(J2)=PSUN(J1)+Q1*Q2
      IF(ABS(X4/PSUN(J2)-1.0).LE.1.0E-5)GO TO 380
      K=K+1
      IF(K.LE.10)GO TO 360
      IFATL=5
      GO TO 410
      IF(J2.EQ.1)GO TO 400
      IF(J2.EQ.1)STRMS)GO TO 390
      J1=J2
      GO TO 360
      J1=IMID
      JSTEP=-1
      GO TO 350
      GO 410 J=1,NSTRMS
      VZON(J)=V7UP(J)+(VZFUN(J)-(PSUN(J)-PSUP(J))/JUG5(HSUP(J),SUP(J))*J
1) /VZUP(J)
      HSDN(J)=HSDN(J)**2+VWUN(J)**2/(2.0*G*EJ)
      IF(HSDN(J).GE.H4IH)GO TO 410
      IFATL=7
      GO TO 600
      HSDN(J)=UDG3(HSDN(J),HSDN(J))
      XX1(1)=0.0
      GO 420 J=1,ITUB
      XX1(J+1)=XX1(J)+(R(J+1)**2-R(J)**2)*(VZON(J+1)+VZON(J))*UDG5(HSDN
1(J)+HSDN(J+1))*0.5,(SDH(J)+SDH(J+1))*0.5)
      G1=XX1(NSTRMS)
      IF(ABS(Q1/FLW-1.0).LE.1.0E-5.AND.KK.GT.1)GO TO 450
      IF(KK.LE.15)GO TO 430
      IFATL=8
      GO TO 600
      Q2=UDG9(HSDN(IMID),SDN(IMID),VZON(IMID)**2)
      G1=(Q1-FLW)*PSUN(IMID)+Q2/(FLOW*(1.0-Q2))
      GO 440 J=1,NSTRMS
      PSUN(J)=PSUN(J)+Q1
      KK=KK+1
      GO TO 340
      IF(KSTEP.EQ.1)STEP)GO TO 510
      GO 500 J=1,NSTRMS
      PSUN(J)=PSUN(J)
      HSUP(J)=HSDN(J)
      VZUP(J)=VZON(J)
      VWUP(J)=VWUN(J)
      HSUP(J)=HSDN(J)
      KSTEP=KSTEP+1
      GO TO 130
      GO 520 J=1,NSTRMS

```



```

H(J)=HON(J)
S(J)=SUN(J)
VW(J)=VWH(J)
RETURN
CALL U00303(LNCI,1)
WRITE(LCG2,610)IFAIL
FORMAT(5X,30HYIXING CALCULATION FAILURE NO.,I2)
RETURN
END

```

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[illegible]


```

SUBROUTINE U0302(R1,R2,X1,X2,M,S,VM,IB1,IB2,M,XK,SCLFAC,SPEED,SPU
1FAC,G,CJ,MIN,NSTR,XS,PI)
DIMENSION R1(1),R2(1),X1(1),X2(1),M(1),S(1),VM(1),IB1(1),IB2(1),W(
11)
DIMENSION X(150),W2D(150),W3D(150),XX1(150),XX2(150),XX3(150),XX5(
19,G),B(150)
19,9)IVALUENCE=(XX2(1),XX5(1))
NTUB=NSTRMS-1
DO 50 J=1,NSTRMS
G1=H(J)-VM(J)*2*(1.0+(IB2(J)+R2(J)*SPEED*SPDFAC*PI/(SCLFAC*30.0)*V
1Y(J)))*2)/(2.0*G*EJ)
IF(Q1.LT.HMI)Q1=H4IN
XX1(J)=U0301(R2,X1,NSTRMS,R2,Q1,XX3,NSTRMS,0,1)
CALL U0301(R2,X1,NSTRMS,R2,Q1,XX3,NSTRMS,0,1)
DO 60 J=1,NSTRMS
XX1(J)=XX3(J)*G/XX2(J)
G1=(R2(NSTRMS)-R2(1))/149.0
711)=R2(1),150
DO 70 J=2,150
71J)=R(J-1)+Q1
CALL U0301(R2,XX1,NSTRMS,R,XX2,Q1,150,0,J)
DO 80 J=1,NSTRMS
XX3(J)=(R2(J)-R1(J))*2+(X2(J)-X1(J))*2*(1.0+(IB1(J)+IB2(J))*0
15)*2)
CALL U0301(R2,XX3,NSTRMS,R,XX1,Q1,150,0,0)
DO 90 J=1,NSTRMS
W2D(J)=VM(J)*2*(1.0+IB2(J))*2)
CALL U0301(R2,W2D,NSTRMS,R,X3,Q1,150,0,0)
CALL U0301(R2,W,NSTRMS,R,W2D,Q1,150,0,0)
NSTRMS=150
NTUB=149
Q2=(SPDFAC*PI/(30.0*SCLFAC))*2
DO 100 J=1,NSTRMS
W3D(J)=0.0
B(1)=(R(2)-R(1))/2.0
B(NSTRMS)=(R(NTUB)-R(1))/2.0
DO 110 J=2,NTUB
B(J)=(R(J+1)-B(J-1))/2.0
DO 270 J=1,NSTRMS
XK=X1(J)/XX3(J)*(Q2*R(J)-XX2(J))
IF(OR)133,12J,200
W3D(J)=W3D(J)+W2D(J)
DO 270 J=1,NSTRMS
IF(J.EQ.1)GO TO 120
IF(J.EQ.150)GO TO 160
DO 140 JJ=2,J
JJ=J-JJ+1
IF(P(J)+DR.GE.R(JJJ))GO TO 150

```

```

140  CONTINUE=
150  JJJ=JJJ+1
160  J1=W20(J)*3(J)/(3(J)-DR)
170  JJ=JJJ,J
180  W30(JJ)=W30(JJ)+J1
190  GO TO 270
200  A=B(J)*W20(J)/(R(NSTRMS)-R(1))
210  IF(J.NE.NSTRMS)A=B(J)*W20(J)/(R(J+1)+R(J))*0.5-R(1)
220  GO TO 270
230  IF(J.EQ.NSTRMS)GO TO 120
240  IF(R(J)+UF.GE.R(NSTRMS))GO TO 250
250  GO TO 210 JJ=J,NSTRMS
260  IF(R(JJ)+DF.LT.R(JJ))GO TO 220
270  CONTINUE=
280  JJ=JJ-1
290  J1=W20(J)*3(J)/(3(J)+DR)
300  JJ=JJ,J
310  W30(JJ)=W30(JJ)+J1
320  GO TO 270
330  A=B(J)*W20(J)/(R(NSTRMS)-R(1))
340  IF(J.NE.1)A=3(J)*W20(J)/(R(NSTRMS)-(R(J)+R(J-1))*J.5)
350  GO TO 260 JJ=J,NSTRMS
360  W30(JJ)=W30(JJ)+A
370  CONTINUE=NSTRMS
380  XX1(1)=0.0
390  DO 280 LL=1,150
400  XX1(LL)=XX1(LL)+W30(LL)
410  XX1(LL)=0.0
420  LL=1,150
430  XX1(LL)=XX1(LL)+R(LL)**(L-1)*W30(LL)
440  DO 330 L=1,9
450  IF(J.LG.1)GO TO 310
460  XX5(L,J)=0.0
470  XX5(L,J)=1,150
480  XX5(L,J)=XX5(L,J)+R(LL)**(L+J-2)
490  GO TO 320
500  XX5(1,1)=150
510  XX5(J,L)=XX5(L,J)
520  CONTINUE
530  CALL UD030(XX5,A1)
540  J=1,NSTRMS
550  W(J)=((XX1(3)*R2(J)+XX1(7))*R2(J)+XX1(6))*R2(J)
560  W(J)=((XX1(4)*R2(J)+XX1(3))*R2(J)+XX1(2))*R2(J)+XX1(1)
570  1+XX1(5))*R2(J)
580  RETURN
590  END

```

```

100 SUBROUTINE UJ330(A,B)
110 DIMENSION A(9,9),B(9),INDEX(9)
      N=9
      DO 100 J=1,N
      INDEX(J)=0
      AMAX=-1.0
      DO 120 J=1,N
      IF (INDEX(J).NE.0) GO TO 120
      DO 115 L=1,N
      IF (INDEX(L).NE.0) GO TO 115
      IFV=ABS(A(J,L))
      IF (PV.LE.AMAX) GO TO 115
      IFV=J
      IF (L.E.AMAX) GO TO 115
      AMAX=PV
      CONTINUE
      IF (AMAX.LL.0.0) RETJRN
      IF (INDEX(AMAX).EQ.0) GO TO 150
      GO 140 L=1,N
      PV=A(AMAX,L)
      A(AMAX,L)=A(AMAX,L)*PV
      IF (L.GT.1) GO TO 140
      IFV=AMAX
      IF (IR)=B(AMAX)
      IF (IC)=PV
      IF (CONV=1.0/A(AMAX,IC))
      A(AMAX,IC)=1.0
      GO 160 L=1,N
      IF (IC.LT.1) GO TO 160
      IF (IC)=B(AMAX)
      CONTINUE
      DO 180 L=1,N
      IF (L.EQ.1) GO TO 180
      IFV=A(L,IC)
      A(L,IC)=0.0
      DO 170 L=1,N
      A(L,IC)=A(L,IC)-A(AMAX,L)*PV
      IF (L)=B(AMAX)
      CONTINUE
      GO TO 110
      END

```


[illegible]

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100 170 180 190 200 210 220 230 240 250 260 270 280 290 300 310 320 330 340 350 360 370
X3=H(J,L2)-(V(J,L2)**2-(VW(J,L2)-XN*P(J,L2))**2)/(2.0*G*EJ)
IF(X2.LT.HMIN)X2=HMIN
IF(X3.LT.HMIN)X3=HMIN
X4=1.0-LOSS(J)/UDG4(X1,S(J,L1))*(UDG4(X3,S(J,L2))-UDG4(X2,S(J,L2)))
1) GO TO 170
X4=1.0
H(J,I)=UDG2(S(J,L1),WORK(J)/X4)
S(J,I)=UDG3(WORK(J),H(J,I))
GO TO 230
CO 200 J=1,NSTRMS
H(J,I)=H(J,L1)+(UDG2(S(J,L1),WORK(J))-H(J,L1))/LOSS(J)
S(J,I)=UDG3(WORK(J),H(J,I))
GO TO 230
CO 220 J=1,NSTRMS
S(J,I)=S(J,L1)+LOSS(J)
H(J,I)=UDG2(S(J,I),WORK(J))
CO 240 J=1,NSTRMS
VW(J,I)=(XN*PIM1(J)*VW(J,I-1)+(H(J,I)-H(J,I-1))*G*EJ)/(XN*P(J,I))
GO TO 270
CO 250 J=1,NSTRMS
H(J,I)=WORK(J)
VW(J,I)=(XN*PIM1(J)*VW(J,I-1)+(H(J,I)-H(J,I-1))*G*EJ)/(XN*P(J,I))
GO TO 330
CO 280 J=1,NSTRMS
VW(J,I)=WORK(J)/P(J,I)
GO TO 310
CO 300 J=1,NSTRMS
VW(J,I)=WORK(J)
CO 320 J=1,NSTRMS
H(J,I)=H(J,I-1)+XN*(R(J,I)*VW(J,I)-PIM1(J)*VW(J,I-1))/(G*EJ)
GO TO (340,400,420,340),IL
IF(L2.EQ.1)GO TO 370
CO 350 J=1,NSTRMS
IF(IPASS.EQ.1.AND.IER.EQ.0)GO TO 350
IF(ITER.EQ.0)V(J,I)=VW(J,I)
X1=H(J,I)-(V(J,I)**2+VW(J,I)**2)/(2.0*G*EJ)
X2=H(J,I)-(VW(J,I)**2-(VW(J,I)-XN*P(J,I))**2)/(2.0*G*EJ)
IF(X1.LT.HMIN)X1=H4IN
IF(X2.LT.H4IN)X2=HMIN
X3=1.0/(1.0+LOSS(J)*(1.0-UDG4(X1,S(J,I))/UDG4(X2,S(J,I))))
GO TO 360
X3=1.0
S(J,I)=UDG3(X3*UDG4(H(J,I),S(J,L1)),H(J,I))
GO TO 270
CO 390 J=1,NSTRMS
IF(IPASS.EQ.1.AND.L2.GT.I)GO TO 380
X1=H(J,L1)-(VW(J,L1)**2-(VW(J,L1)-XN*P(J,L1))**2)/(2.0*G*EJ)
1) IF(X1.LT.H4IN)X1=H4IN

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330 X2=H(J,L2)-(V*(J,L2)**2+VM(J,L2)**2)/(2.0*G*EJ)
340 X3=H(J,L2)-(V*(J,L2)**2-(VM(J,L2)-XN*R(J,L2))**2)/(2.0*G*EJ)
400 IF(X2.LT.HMIN)X2=HMIN
410 IF(X3.LT.HMIN)X3=HMIN
420 X4=1.0-LOSS(J)/UDG+(X1,S(J,L1))*(UDG4(X1,S(J,L2))-UDG4(X2,S(J,L2)))
430 GO TO 390
440 X4=1.0
450 S(J,I)=UDG3(X4,UDG+(H(J,I),S(J,L1)),H(J,I))
460 GO TO 570
470 J=1,NSTRMS
480 S(J,I)=UDG3(UDG+(H(J,L1)+LOSS(J)*(H(J,I)-H(J,L1)),S(J,L1)),H(J,I))
490 GO TO 570
500 J=1,NSTRMS
510 S(J,I)=UDG3(X1,L1)+LOSS(J)
520 GO TO 570
530 J=1,NSTRMS
540 X1(J,I)=H(J,I-1)-XN*RIM1(J)*VM(J,I-1)/(G*EJ)
550 IF(L2.NE.I)GO TO 430
560 IF(IPASS.EQ.1.AND.IITER.EQ.0)GO TO 470
570 IF(ITER.EQ.0)VV(J)=VM(J,I)
580 X2=X1(J)+(XN*R(J,I))**2/(2.0*G*EJ)
590 X1=X2-VV(J)**2*(1.0+TBETA(J,I))**2/(2.0*G*EJ)
600 IF(X1.LT.HMIN)X1=HMIN
610 IF(X2.LT.HMIN)X2=HMIN
620 X3=1.0/(1.0+LOSS(J)*(1.0-UDG4(X1,S(J,I))/UDG4(X2,S(J,I))))
630 X3=1.0
640 S(J,I)=UDG3(X3*UDG+(X2,S(J,L1)),X2)
650 GO TO 570
660 J=1,NSTRMS
670 X4=X1(J)+(XN*R(J,I))**2/(2.0*G*EJ)
680 IF(X4.LT.HMIN)X4=HMIN
690 X1=UDG4(X4,S(J,L1))
700 IF(IPASS.EQ.1.AND.L2.GT.I)GO TO 500
710 X2=X1(J)+(XN*R(J,L2))**2/(2.0*G*EJ)
720 X3=H(J,L2)-(V*(J,L2)**2+VM(J,L2)**2)/(2.0*G*EJ)
730 IF(X2.LT.HMIN)X2=HMIN
740 IF(X3.LT.HMIN)X3=HMIN
750 X4=X1-LOSS(J)*(UDG4(X2,S(J,L2))-UDG4(X3,S(J,L2)))
760 S(J,I)=UDG3(X1,X4)
770 GO TO 570
780 IF(IPASS.EQ.1.AND.IITER.EQ.0)GO TO 530
790 J=1,NSTRMS
800 IF(ITER.EQ.0)VV(J)=VM(J,I)
810 X1=H(J,I-1)+X4*(VV(J)*(TBETA(J,I)+XN*R(J,I)/VV(J))*R(J,I)-RIM1(J))*
820 VV(J,I-1)/(G*EJ)
830 IF(X1.LT.HMIN)X1=HMIN

```



```

160 GO TO 200
170 DO J=1,NSTRMS
180 XX2(J)=XL(J,L1)
190 XX6(J)=XL(J,I)/XL(NSTRMS,I)
200 L2=IS2(I)
CALL UD0301(STATAC(L2),DATA5(L2),NDATA(I),XX6,SOL,X1,NSTRMS,INTERP(I),0)
1)0)
IF(SP=ED(I).:I.0.0)GO TO 208
IF(SP=ED(I).:I.0.0)GO TO 208
IF(I.I.LT.3)GO TO 203
II=I-1
IF(SP=ED(II).NE.0.0)GO TO 205
IF(I.I.EQ.2)GO TO 208
II=II-1
GO TO 204
IF(SP=ED(I).LT.0.0)Q=-1.0
GO TO 203
Q=-1.0
GO TO 210
TALPH1(J)=(VM(J,L1)-XN*R(J,L1))/VM(J,L1)
CIF(J)=(1.0-VM(J,I)/VM(J,L1))*SQR((1.0+TBETA(J,I)**2)/(1.0+TALPH1(J)**2))
1) *SQR((1.0+TALPH1(J)**2))*Q
2) L2=ABS(FLOAT(NEVAL(I)))
L3=N)IFF(L2)
CALL UD0301(DIFF(1,L2),F0HUB(1,L2),L3,UIF,XX3,X1,NSTRMS,0.0)
CALL UD0301(DIFF(1,L2),F0MID(1,L2),L3,DIF,XX4,X1,NSTRMS,0.0)
CALL UD0301(DIFF(1,L2),F0TIP(1,L2),L3,DIF,XX5,X1,NSTRMS,0.0)
XX1(1)=0.1
XX1(2)=0.5
XX1(3)=0.9
XX0 220 J=1,NSTRMS
XX1(4)=XX3(J)
XX1(5)=XX4(J)
XX1(6)=XX5(J)
X1=(R(J,I)-R(1,I))/R(NSTRMS,I)-R(1,I)
CALL UD0301(XX1,XX1(4),3,X1,WPARA(J),X1,1.0,0)
GO 230 J=1,NSTRMS
XMR(J)=0.0
HNGH(J)=0.0
XINC(J)=0.0
XINC1(J)=0.0
WPARA(J)=WPARA(J)*2.0*SOL(J)*SQR((1.0+TBETA(J,I)**2)
WU(J)=WPARA(J)*2.0*SOL(J)*SQR((1.0+TBETA(J,I)**2)

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```

230      WT(J)=W(J)
      IF(NDEL(I).F).0)GO TO 384
      L2=IS3(I)
      CALL UD0301(DEL(L2),DELTA(L2),NDEL(I),XX2,P41,X1,NSTRMS,1,0)
      IF(NDATA(L1).F).0)GO TO 340
      CALL UD0301(R(I,L1),NSTRMS,P(1,L1),X1,XX1,NSTRMS,0,1)
      L2=NDIX=N(L1)+1
      GO TO(240,260,280,300),L2
240      J=1,NSTRMS
250      XX2(J)=R(J,L1)
      GO TO 320
260      J=1,NSTRMS
270      XX2(J)=R(J,L1)/R(J,NSTRMS)
      GO TO 320
280      J=1,NSTRMS
290      XX2(J)=XL(J,L1)
      GO TO 320
300      J=1,NSTRMS
310      XX2(J)=XL(J,L1)/XL(NSTRMS,L1)
      L2=IS2(L1)
      L3=NDAT4(L1)
      CALL UD0301(ATA(L2),DATA1(L2),L3,XX2,XX3,X1,NSTRMS,INTERP(L1),J)
      DO 330 J=1,NSTRMS
      X1=ATAN(R(J,L1+1)-R(J,L1))/(X(J,L1+1)-X(J,L1))+ATAN(R(J,L1)-R(
      BETAL(J)=ATAN((TAN(XX3(J)/C1)*(1.0-XX1(J)*TAN(X1))-TAN(XX4
      1(J)/C1))+SORT(1.0+XX1(J)*2)+COS(X1))
      1(XINC(J))=ATAN(1ALPH1(J))-BETAL(J)*0
      DO 380 J=1,NSTRMS
      ANG(J)=XINC(J)+PM1(J)/C1
      X1=H(J,L1)-(VX(J,L1)*2+VM(J,L1)*2)/(2.0*G*EJ)
      IF(X1.LT.HMI)X1=HMIN
      X4=UDG8(X1,S(J,L1))
      X2=(X4+1.0)/(X4-1.0)
      X3=UDG9(X1,S(J,L1),VM(J,L1)*2*(1.0+TALPH1(J)*2))
      XMR(J)=SORT(X3)
      X5=X4
      IF(X6.LT.1.0)X6=1.0
      X7=X3+ATAN(SQRT(X6-1.0)/X3)-ATAN(SQRT(X6-1.0))+ANG(J)
      X10=0.0
      IF(X7.LT.0.0)GO TO 375
      X8=0.0+PI*(X3-1.0)
      IF(X7.GT.X8)GO TO 374
      X9=UDG9(X6-1.0)+0.1
      K=1
      X10=X9-(X2+X3)*X9*(1.0+X9*X9)/(X9*X9*(X2-1.0))*(X3*ATAN(X9/X3)-ATA
      1N(X9)-X7)
      IF(ARS(X10-X3).LE.0.0001)GO TO 376

```

```

360 IF(K.GT.2)GO TO 360
K=K+1
X9=X10
GO TO PRINT, LG, 0)GO TO 374
CALL UD0303(LNCT, 1)
WRITE(LOG2, 370)IPASS, I, J
FORMAT(5X, 4H PASS, I3, 9H STATION, I3, 5H STREAMLINE, I3, 5H PRANDTL
FOR MERGE FUNCTION NOT CONVERGED - USE INLET MACH NO)
1 X10=SQRT(X6-1.0)
HIGH(J)=SQRT(1.0+X10*X10)
X1=(HIGH(J)+SQRT(X6))/2.0
IF(X5.LI.1.0)X1=X1*SQRT(X5)
IF(X1.LI.1.0)GO TO 383
X1=X1+X1
XS(J)=((X4+1.0)*X1/(X4-1.0)*X1+2.0))*X4/(X4-1.0))*(X4+1.0)/(2.0*X5))*X4
2/(1.0-X4)-1.0)
1.0*X4-X1-X4+1.0))*X4/(X4-1.0)/(1.0+(X4-1.0)/2.0*X5))*X4
383 IF(IPRINT.EQ.1)GO TO 400
L2=IS2(I)
L3=INTERP(I)
IF(NDATA(I).GE.5)
1 CALL UD0301(DATAC(L2), L4, XX6, XX5, X1, NSTRMS, L3, 0)
CALL UD0301(DATAC(L2), L4, XX6, XX1, X1, NSTRMS, L3, 0)
CALL UD0301(DATAC(L2), L4, XX6, XX3, X1, NSTRMS, L3, 0)
NDATA(I)=NSTRMS
L2=L2-1
L3=L3-1
J=1, NSTRMS
X=L2+J
IF(NDATA(I).GE.5)
1 DATAC(K)=XX6(J)
IF(NDATA(I).GE.5)
1 DATAC(K)=XX5(J)
IF(MT(J).GT.WMAX)MT(J)=WMAX
1 DATAC(K)=WT(J)
DATAC(K)=XX3(J)
DATAC(K)=XX4(J)
DATAC(K)=XXL(J)
GO TO 420
IF(LNCT+3.LE.NPAGE)GO TO 420
WRITE(LOG2, 410)
FORMAT(1H1)
FORTE=+NSTRMS
1 FNCTE(LO2, 430)
FORMAT(5X, 12H STREAM INLET OUTLET CASCADE DIFF EXPANDED SHOCK LOSS TOT
101 FUSION, 12H BLADE INLET EXPANSION INLET FACTOR PARAMETER TOT
2 AL, /, 5X, 12H LINE RADIUS RADIUS RADIUS SOLIDITY

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3 LOSS      ANGLE      ANGLE      ANGLE      M.NO      MACH NO      LOSS      LOSS
4,7,2X)
LNCI=LNCI+3
DO 440 J=1,N3IRMS
X1=RTAI(J)*C1*9
X2=XINC(J)*C1
X3=XINC(J)*C1
WRITE(LUS2,460)J,R(J,L1),R(J,I),SOL(J),DIF(J),WPARA(J),WD(J),X1,X2
1,X3,XMR(J),HIGH(J),WT(J)
CONTINUE
FORMAT(I9,F1J.3,F3.3,2F9.4,F10.5,F9.5,2F9.3,F10.3,F10.4,F6.4,F8.5,
1F9.5)
END
END

```

440

450

460


```

130      GO 140 J=1, NSIRMS
      X1=SQRT((K(J,I+1)-R(J,I))**2+(X(J,I+1)-X(J,I))**2)
      X2=SQRT((K(J,I)-R(J,I-1))**2+(X(J,I)-X(J,I-1))**2)
      X3=ATAN2(R(J,I)-R(J,I-1),X(J,I)-X(J,I-1))
      X4=ATAN2(R(J,I)-R(J,I+1),X(J,I)-X(J,I+1))
      CR(J)=(X3-X4)/(X1+X2)*2.0
      IF(CR(J).NE.0.0)CR(J)=1.0/CR(J)
      PHI(J)=(X3+X4)/2.0
      VA=VM(J,I)*COS(PHI(J))
      VK=VM(J,I)*SIN(PHI(J))
      FI=PHI(J)*C1
      GA=ATAN(GAMA(J))*C1
      FPG(J)=FI+GA
      V(J)=SQRT(VM(J,I)**2+VM(J,I)**2)
      WPT(J)=LOG2(1.78)*J,R(J,I),X(J,I),VM(J,I),VA,VK,V(J),
140      CR(J),FI,GA
      CALL UO33C(19,33,140)
      WRITE(19,33) STREAM,7X,4HMMACH,6X,4(1H-),3HPRESSURES,4(1H-),5X,17H---
150      1- LINE,4HFLOW,3X,11H(3H+GAMMA),7,7H -LINE,7X,8HNUMBER,5X,5HTOTAL,6X,17H---
      2- 6HSTATIC,5X,6HSTATIC,5X,6HWEIGHT,5X,5HTOTAL,6X,6HSTATI
      3- CO,16X,5HANGLE,7,2X)
      DELT3(J)=0.0
      H3=H(J,I)-V(J)*2/(2.0*G*EJ)
      IF(H3.LT.H4IN)H3=H4IN
      XM(J)=SQRT(U3G9(H3,S(J,I),V(J)**2))
      FT(J)=UUG4(H(J,I),S(J,I))
      FTINS=PT(J)/SCLFAC**2
      PSINS=PS(J)/SCLFAC**2
      TT=UUG7(H(J,I),S(J,I))
      T3(J)=UUG7(H3,S(J,I))
      WT(J)=UUG7(H3,S(J,I))
      ALPHA=0.0
      IF(I.NE.1)STAG=OR(J,NE.1)ALPHA=C1*ATAN(VM(J,I)/VM(J,I))
      WRITE(19,33) J,X1(J),PTINS,PSINS,TT,TS(J),H(J,I),HS,S(J,I)
190      1- ALPHA,25G(J)
      FOMAT(15,E1+4,2F11.3,F12.6,F10.3,F11.3,F12.6,F10.3,F11.3)
200      IF(I.NE.1)3C IN 220
      F13AR=0.0
      F13AR=0.0
      H4I(1)=PT(1)
      H4I(210)=PT(J+1)
      CR1(J+1)=PT(J+1)
      XI=(DELF(J+1)-DELF(J))/2.0
      P13AR=P13AR+X1*(PT(J)+PT(J+1))

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```

410 IF (SOLID(J).EQ.0) GO TO 410
X2=VM(J,L1)-XN*R(J,L1)
X1=SQRT(VM(J,L1)**2+X2**2)
X3=VM(J,I)-U
UPRL1=1.0-VF/X1+(X2-X3)/(2.0*X1*SOLID(J))*Q
PSL1=PSL2
IF (L2.EQ.L1) GO TO +20
PSL1=H(J,L1)-(VM(J,L1)**2+VM(J,L1)**2)/(2.0*G*EJ)
PSL1=PSL1+(V4(J,L1)*+2+(VM(J,L1)-XN*R(J,L1))*+2)/(2.0*G*EJ)
PSL1=UDG4(PSL1,S(J,L1))
PSL1=UDG4(PRL1,S(J,L1))
PR1=UDG4(PRL1,S(J,L1))
PR1=(PS(J)-PSL1)/(PRL1-PSL1)
WRITE(LOG2,434) J,U,VZ,XMR,BETA,VELTB(J),BETA,TANEPS(J),DELP,COEF,
10 IF,OPD
FORMAT(I6,F11.2,F11.2,F11.4,4,F11.3,F11.4,F11.5,F11.4,F11.4)
CALL UD0303(LNCT,NSTR4S+5)
PBAR=0.0
GO 440 J=1,I,TUB
X1=(DELF(J+1)-DELF(J))/2.0
PBAR=PBAR+X1*(PT(J)+PT(J+1))
HBAR=HBAR+X1*(H(J,I)+H(J+1,I))
GBAR1=PBAR/PBAR
CH1=(HBAR-H1BAR)/H1BAR
EFF1=0.0
IF (HBAR.NE.H1BAR) EFF1=(UDG2(S1BAR,PAR)-H1BAR)/(H3AR-H1BAR)
OPPR=GBAR1
IF (EFF1.NE.0.0) EFF=EFF1
IF (L1.EQ.LIKEP) GO TO 460
LIKEP=0.0
HNBAR=0.0
GO 444 J=1,NSTR4S
UDG4(H(J,L1),S(J,L1))
GO 450 J=1,I,TUB
X1=(DELF(J+1)-DELF(J))/2.0
PBAR=PBAR+X1*(PN(J)+PN(J+1))
HNBAR=HNBAR+X1*(H(J,L1)+H(J+1,L1))
SN3AP=UDG3(PV3AR,H1BAR)
EFFN=0.0
IF (HNBAR.NE.H3AR) EFFN=(UDG2(SNBAR,PBAP)-HNBAR)/(H8AR-HNBAR)
P3AR=PBAP/PV3AP
CHN=(HBAR-HNBAR)/HNBAR
WRITE(LOG2,470) I,L1,I,I,L1,I,I,RBAR1,RBARN,EFF1,EFFN,OH1,OHN,
FORMAT(I2X,/,3H STATION,/,13H MEAN VALUES,/,13H INLET TO STA,/,7H
1,13,16H THROUGH STATION,/,12,/,7H -LINE,/,6X,81HPRESSURE RATIO,
22,7H STA,/,12,/,9H PRESSURE EFFICIENCY ON H
30, DELTA H, PRESSURE RATIO
4.4, F19.4,/,13X,74H RATIO EFFICIENCY

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SACV ON H1      IS-V EFFY,2F19.4,/,8CX,13HDELTA H ON H1,F15.4,F19.4
C40 490 J=1,NSTPM5
RBAFI=PT(J)/PI(J)
EFFI=0.0
IF (H(J,I).NE.H(J,1))EFFI=(UDG2(S(J,1),PT(J))-H(J,1))/(H(J,1))-H(J,1)
1))
CH1=(H(J,I)-H(J,1))/H(J,1)
RBAFI=PT(J)/PI(J)
EFFN=0.0
IF (H(J,I).NE.H(J,1))EFFN=(UDG2(S(J,1),PT(J))-H(J,1))/(H(J,1))-H(J,1)
1J,L1))
CH1=(H(J,I)-H(J,L1))/H(J,L1)
WRITE(LOG2,43J)J,RBAFI,EFFI,OH1,RBAFN,EFFN,OH1
FORMAT(I6,F14.4,F10.4,F11.4,F10.4,F11.4)
IF (IFL-EL.0)GO TO 700
CALL UDG33(LNCT,NSTPM5+8)
XN=SPI=0(I+1)*SPDFAC(ICASE)
IP=I+1
XBLADE=1.0
IF (XBLADE(IP).NE.0)XBLADE=ABS(FLOAT(NBLADE(IP)))
L1=XBLADE
WRITE(LOG2,51J)I,XJ,L1
FORMAT(I2X,/,10X,7HSTATION,13,46H IS AT THE LEADING EDGE OF A BLADE
ROTATION,3 AT,19,1,14 RPM NUMBER OF BLADES IN ROW=,13,/,10X,99(I
XJ,/,33H STREAM BLADE PRESS DIFF,/,100H -LINE ANGLE
SINGIDENCE VELOCITY MACH NO. FLOW ANGLE
L1=XN*PI/(30.0*SCLFAC)
XC=1.0
IF (SP=EU(IP).LT.0.0)GO TO 520
IF (SP=EU(IP).GT.0.0)GO TO 540
IF (IP.LT.1)GO TO 550
IF (IP=1)
IF (SP=EU(1).LT.0.0)GO TO 530
IF (II=1)
IF (II=1)
IF (SP=EU(II).LT.0.0)Q=-1.0
IF (II=1)
IF (SP=EU(II).LT.0.0)Q=-1.0
GO TO 520
GO TO 550
GO 500 J=1,NSTPM5
CR(J)=0.0
TANEP5(J)=0.0
IF (NWORK(I).NE.0.0)DATA(I).=Q.0)GO TO 660
L1=NDIMEN(I)+1
GO TO(570,580,610,630),L1
C40 580 J=1,NSTPM5
TANEP5(J)=R(J,I)

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590      TO 650 J=1,NSTRMS
600      TANEPS(J)=P(J,I)/R(NSTRMS,I)
610      GO TO 650
620      J=1,NSTRMS
630      TANEPS(J)=XL(J,I)
640      J=1,NSTRMS
650      TANEPS(J)=XL(J,I)/XL(NSTRMS,I)
660      CALL UD0301 (DATA(L1),DATA1(L1),NDATA(I),TANEPS,CR,X1,NSTRMS,INTERP,
1      (I),0)
1      CALL UD0301 (DATA(L1),DATA3(L1),NDATA(I),TANEPS,X1,NSTRMS,N
1      BETA=0.0
670      GO 680 J=1,NSTRMS
680      U=XN*P(J,I)**2+(VM(J,I)-U)**2
690      VM=XN*P(J,I)*V/J(J)
700      BETA=ATAN(VM(J,I)-U)/VM(J,I))*C1
710      IE(MWORK(I))=0
720      BETA=ATAN((TAN(CR(J)/C1)*(1.0-GAMA(J))*TAN(PHI(J)))-TAN(PHI(J)))*C1
730      IN(1,TANPS(J)/C1)*SQRT(1.0+GAMA(J)**2))*COS(PHI(J))*C1
740      X1=SQRT((BETA-33.33)*9
750      DELP=PI*(R(J,I)**2.0*W(J)/(SCLFAC**2*XELADE*G))*(SIN(BETA/C1)*COS(BE
1      TA/C1)*G*(J,I)+1)*S(J,I+1)-S(J,I))/X1+VM(J,I)*(R(J,I)+X1)**2)
2      *VM(J,I)+1)*R(J,I)*VM(J,I))
680      DELT=LOG2(633)J,U,VR,XMR,BETA,DELTF(J),RBETA,TANEPS(J),DELP
690      FOMAT(10,F1+2,F11.2,F11.4,4F11.3,F11.4)
700      CONTINUE
710      IF(NEL=J,0)GO TO 770
720      L1=(ILAST-1)/10+1
730      CALL UD0303(LNCT,3+5*L1)
740      FOMAT(12,X/,10X,7(1H*))
750      DO 720 X=1,L1
760      L2=10+(X-1)+1
770      L3=12+9
780      IF(L3.GT.ILAST)L3=ILAST
790      WRITE(LOG2,730) (I,I=L2,L3)
800      WRITE(LOG2,740) (DELH(I),I=L2,L3)
810      WRITE(LOG2,750) (Q(LY(I),I=L2,L3)
820      WRITE(LOG2,760) (HW3L(I),NUMBER,14X,10I10)
830      FOMAT(12,X/,10X,7(1H*))
840      FOMAT(12,X/,10X,7(1H*))
850      FOMAT(12,X/,10X,7(1H*))
860      FOMAT(12,X/,10X,7(1H*))
870      FOMAT(12,X/,10X,7(1H*))
880      FOMAT(12,X/,10X,7(1H*))
890      FOMAT(12,X/,10X,7(1H*))
900      FOMAT(12,X/,10X,7(1H*))
910      FOMAT(12,X/,10X,7(1H*))
920      FOMAT(12,X/,10X,7(1H*))
930      FOMAT(12,X/,10X,7(1H*))
940      FOMAT(12,X/,10X,7(1H*))
950      FOMAT(12,X/,10X,7(1H*))
960      FOMAT(12,X/,10X,7(1H*))
970      FOMAT(12,X/,10X,7(1H*))
980      FOMAT(12,X/,10X,7(1H*))
990      FOMAT(12,X/,10X,7(1H*))

```

10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52


```

COMMON/GAS/G, T, J, P, CP, GAMMA, R0JCP
DOGG=GA 144
RETURN
FUNCTION UJG3(H, S, V2)
COMMON/GAS/G, T, J, P, CP, GAMMA, R0JCP
DOGG=CP+V2/(GAMMA+G+R*H)
RETURN
END

```

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NNNNNNNNNN
NNNNNNNNNN
NNNNNNNNNN
NNNNNNNNNN
NNNNNNNNNN
NNNNNNNNNN
NNNNNNNNNN
NNNNNNNNNN

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365 L=11,11,11
370 LINE(L)=X1
380 GO TO 650
390 IF (Y1(I)-X1)*YH+YINC2*OR.Y1(I).LE.YH-YINC2)GO TO 630
400 L=(X1(I)-X1)/XRANGE+120.0+1.5
410 LINE(L)=SYM2JL( 1)
420 CONTINUE
430 IF (KLINR.EQ.1.0*KLIN.EQ.0.7*OR.KLIN.EQ.0.13*OR.KLIN.EQ.0.43*OR.KLIN.EQ.0.49
440 1.-OR.KLIN.EQ.0.31*OR.KLIN.EQ.0.37*OR.KLIN.EQ.0.43*OR.KLIN.EQ.0.49)
450 2.*X1TE(LOG1,61J)LINE
460 3.FORMAT(IX,12141)
470 GO TO 750
480 YNUM=YH+10.0**NY
490 WRITE(LOG1,63J)YNUM,LINE
500 FFORMAT(IX,Fc,3,1X,12141)
510 YH=YH-YINC
520 XNUM(1)=X1*10.0**HX
530 XINC=((XH-X1)/12.0)*10.0**MX
540 GO 800 I=2,11
550 XNUM(I)=XNUM(I-1)+XINC
560 WRITE(LOG1,63J)XNUM
570 FFORMAT(IX,12(Fc,3,*X),Fc,3)
580 RETURN
590 WRITE(LOG1,91J)
600 FFORMAT(//,35X,5*HNO PLOT HAS BEEN MADE BECAUSE 'X' OP 'Y' RANGE IS
610 1 ZEROC)
620 1 RETURN
630 END

```



```

170      O 180 J=1,NSTRMS
180      XX1(J)=XL(J,I+1)/XL(NSTRMS,I+1)
190      L1=IS2(I+1)
      CALL UD0301 (DATA3(L1),DATA4(L1),NDATA(I+1),XX1,XX1,X1,NSTRMS,INTERP
1      (I+1),0)
      DO 200 J=1,NSTRMS
      LAMIP1(J)=1.-XX1(J)
      DO 220 J=1,NSTRMS
      X1=SQRT((R(J,I+1)-R(J,I))**2+(X(J,I+1)-X(J,I))**2)
      X2=SQRT((R(J,I)-R(J,I+1))**2+(X(J,I)-X(J,I+1))**2)
      X3=ATAN2(R(J,I+1)-R(J,I),X(J,I)-X(J,I+1))
      XH1(J)=(X3+X4)/2.0
      XH2(J)=(X3-X4)/(X1+X2)*2.0
      CRVWDM(J)=0.0
      CLADM(J)=(CL4*IP1(J)-LAM1(J))/X1+(LAMI(J)-LAMIM1(J))/X2/2.0
      IF(IPASS.EQ.1)GO TO 220
      USDM(J)=(S(J,I+1)-S(J,I))/X1+(S(J,I-1)-S(J,I))/X2/2.0*EJ
      CRVWDM(J)=(R(J,I+1)*VM(J,I)-R(J,I)*VM(J,I))/X1+(R(J,I)*VM(J,I)-
1      R(J,I-1)*VM(J,I-1))/X2/(2.0*R(J,I))
      CONTINUE
      IF(IPASS.EQ.1.OR.NDATA(I).EQ.3.OR.NEON.EQ.1.OR.NWORK(I).NE.0.OR.NW
1      ORK(I+1).EQ.1)GO TO 390
      L1=NOIMEN(I)+1
      GO TO(221,223,225,227),L1
      DO 222 J=1,NSTRMS
      TEIP1(J)=R(J,I)
      DO 229 J=1,NSTRMS
      TEIP1(J)=R(J,I)/R(NSTRMS,I)
      DO 226 J=1,NSTRMS
      TEIP1(J)=XL(J,I)
      GO TO 229
      DO 226 J=1,NSTRMS
      TEIP1(J)=XL(J,I)
      GO TO 229
      DO 226 J=1,NSTRMS
      TEIP1(J)=XL(J,I)/XL(NSTRMS,I)
      L1=IS2(I)
      CALL UD0301 (DATA3(L1),DATA4(L1),NDATA(I),TEIP1,TEIP1,X1,NSTRMS,NTE
1      RP(I),0)
      X1=SP2(J(I+1)*SP0FAC(ICASE)*PI/(30.0*SOLFAC)
      DO 230 J=1,NSTRMS
      TEIP1(J)=TAN(TEIP1(J)/C1)
      TBIP1(J)=(VM(J,I)-X1*R(J,I))/VM(J,I)
      DO 240 J=1,NSTRMS
      CLADM(J)=0.0
      CRVWDM(J)=0.0
      CR(J)=0.0
220
221
222
223
224
225
226
227
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229
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245 IF(I.E.G.1)GO TO 244
246 PHI(J)=ATAN2(R(J,1)-XIM1(J),X(J,I)-XIM1(J))
260 GO TO 390
270 J=1,NSTRMS
280 PHI(J)=ATAN2(R(J,2)-R(J,1),X(J,2)-X(J,1))
290 X1(J)=H(J,1)
300 LAMI(J)=1.0
310 LAMIP1(J)=1.0
320 L2=N(I,M,N(2)+1)
330 GO TO(290,310,330,350),L2
340 X1(J)=K(J,2)
350 GO TO 370
360 J=1,NSTRMS
370 X1(J)=X(J,2)/S(NSTRMS,2)
380 GO TO 370
390 J=1,NSTRMS
400 X1(J)=XL(J,2)
410 GO TO 370
420 J=1,NSTRMS
430 X1(J)=XL(J,2)/XL(NSTRMS,2)
440 L1=IS2(2)
450 CALL UD0301(J)ATAC(L1),DATA4(L1),NDATA(2),XX1,XX1,X1,NSTRMS,NTERP(2)
460 J=1,NSTRMS
470 LAMIP1(J)=1.0-X1(J)
480 CALL UD0301(R(1,I),X(1,I),NSTRMS,P(1,I),X1,GAMA,NSTRMS,G,1)
490 GO 400 J=1,NSTRMS
500 GAMA(J)=ATAN(GAMA(J))
510 SPPG(J)=GAMA(J)+PHI(J)
520 SPPG(J)=COS(SPPG(J))
530 VV(J)=SIN(SPPG(J))
540 GO 410 J=1,ITUB
550 SOL(J)=XL(J+1,I)-XL(J,I)
560 GPHIDL(J)=(R(J+1,I)-R(J,I))/DL(J)
570 IF(I.E.0.1)JF=KJDRK(I).GE.5)GO TO 430
580 GO 420 J=1,ITUB
590 VV(J)=VW(J,I)
600 EX1(J)=(VW(J+1,I)+VW(J,I))/(R(J+1,I)+R(J,I))*R(J+1,I)-R(J,I)
610 EX2(J)=(H(J+1,I)-H(J,I))/DL(J)*G*EJ
620 GO 420 J=1,NSTRMS
630 X1=UD069(H(J,I),S(J,I))
640 X1=(2.0/UD069(H(J,I),S(J,I),1.0)-VW(J,I))*2*(X1-1.0)/(X1+1.0)
650 IF(X1.GT.1.0)GO TO 425

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422 IF (IPASS.LE.NFORCE)GO TO 424
    CALL UD0303(LNCT,I)
    WRITE(LOG2,422)IPASS,I,J,X1
    FORMAT(5X,4HPASS,I3,12H STATION,I3,12H
424 1G MERIDIONAL VELOCITY SQUARED =,E12.5)
    X1=625000.0
    IF (IFAILO.EQ.?) IFAILO=I
    VMAX(J)=SQRT(X1)
    GO TO 430
426 DO 440 J=1,ITUR
    FX1(J)=(TETA(J+1,I)+TETA(J,I))/(R(J+1,I)+R(J,I))*TETA
430 1(J+1,I)-R(J,I)*TETA(J,I))/DL(J)
    FX2(J)=(X1(J+1,I)-X1(J))/DL(J)*G*EJ
    DO 446 J=1,NSTRMS
    X1=X1(J)+(XN*F(J,I))*2/(2.0*G*EJ)
    X1=1.0/UD039(X1,S(J,I).1.0)*(1.0+(UDG8(X1,S(J,I))-1.0)*(1.0+TETA(
442 1)F(X1,G1.1.0)GO TO 446
    IF (IPASS.LE.NFORCE)GO TO 442
    CALL UD0303(LNCT,I)
    WRITE(LOG2,422)IPASS,I,J,X1
    X1=625000.0
    IF (IFAILO.EQ.?) IFAILO=I
    VMAX(J)=SQRT(X1)
    VMIN=1.05*VMAX(IMID)
    ITER=0
    IFER=ITER+1
    IFAIL=0
    ICONF1=0
    DO 470 J=1,NSTRMS
    VVOLD(J)=VV(J)
    IF (EQ.1.0P.NWORK(I).GE.5)GO TO 810
    DO 580 J=1,ITUR
    X1=(H(J,I)+H(J+1,I))/2.0-(((VVOLD(J)+VVOLD(J+1))/2.0)**2+((VM(J,I)
470 1+VM(J+1,I))/2.0)**2)/(2.0*G*EJ)
    IF (X1.GE.HMIN)GO TO 520
    IF (IPASS.LE.NFORCE)GO TO 510
    IF (LNCT.LI.NPAGE)GO TO 480
    WRITE(LOG2,500)
    LNCT=LNCT+1
    WRITE(LNCT,1
480 1)
    WRITE(LOG2,430)IPASS,I,ITER,J,X1
    FORMAT(5X,4HPASS,I3,12H STATION,I3,11H ITERATION,I3,12H STREAMTU
490 1BE,I3,53H STATIC ENTHALPY BELOW LIMIT IN MOMENTUM EQUATION AT,E13
    2)
    FORMAT(1H1)
    IFAIL=1
    X1=HMIN
    X2=(S(J,I)+S(J+1,I))/2.0
500
510
520

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530      X9=U0G8(X1,X2)
      X7=U0G7(X1,X2)
      X1=U0G9(X1,X2,((VVOLU(J)+VVOLU(J+1))/2.0)**2)
      XQ=X1
      IF(X1,LE,0.9301)GO TO 560
      IF(IPASS,LE,NFORCE)GO TO 550
      IF(LNCT,LT,NFGE)GO TO 530
      WRITE(L052,5JJ)
      LNCT=LNCT+1
      X1=SCRT(X1)
      *WRITE(L062,5+0)IPASS,I,1,IF,J,X1
      *FORMAT(5X,4H PASS,I3,9H STATJN,I3,11H ITERATION,I3,12H STREAMTU
1000      *E,13,39H MERIDIONAL MACH NUMBER ABOVE LIMIT AT,I13.5)
      IF(4IL=1)
      X1=0.9401
      X2=(CPBG(J)+CPBG(J+1))/2.0
      X3=(CPBG(J)+3*CPBG(J+1))/2.0
      AFUN(J)=-2.0/(1.0-X1)*(1.0-X2*X2*XQ)*(CR(J)+CR(J+1))/(2.0*X2)-X3/
1100      X2*DPHICL(J)-X3*(SIN(PHI(J)+PHI(J+1))/2.0)/(R(J,I)+K(J+1,I))*2.0*
      3Q(LADM(J+1))/(LAMI(J)+LAMI(J+1))
      12(1.0+X1*(VM(J,I)+VM(J+1,I))/(VVOLU(J)+VVOLU(J+1))*2)+(CLADM(J)+
      3Q(LADM(J+1))/2.0*(EX2(J)-X7*DSOL(J)-FX1(J))
      13BFUN(J)=2.0*(EX2(J)-X7*DSOL(J)-FX1(J))
      IF(1,EG,NSTNS,OR,IPASS,EQ,1)GO TO 540
      IF(NEGN,EQ,1)
      10(NEGN,EQ,1)
      IF(NWORK(I),EQ,0.0)
      11(NWORK(I),EQ,0.0)
      IF(NWORK(I),EQ,0.0)GO TO 564
      X4=(TRFAC(J,I)+TBETA(J+1,I))/2.0
      X5=(TANEPS(J)+TANEPS(J+1))/2.0
      3FUN(J)=BFUN(J)+2.0*(X7*(DSOL(J)+DSOL(J+1))/2.0*(X3*(1.0/(1.0+X+
1411      14)+X5*X1/(1.0-X1))-X5*X/(1.0-X+X4))-(VVOLU(J)+VVOLU(J+1))/4.0*(D
      2*VWDM(J)+ORVWDM(J+1))*(X5-X3*X1/(1.0-X1)*X4))
      GO TO 560
      X4=(TBIP1(J)+TBIP1(J+1))*0.5
      X5=(TBIP1(J)+TBIP1(J+1))*0.5
      30 TO 562
      BFUN(J)=BFUN(J)+X7*(DSOL(J)+DSOL(J+1))*X3*(1.0-X1*(X6-1.0))/(1.0-X
1111
      CONTINU=
      VV(IMID)=VVOLU(IMID)**2
      J=IMID
      JINC=1
      JOLD=J
      J=J+JINC
      J=JOLD
      J=JOLD
      IF(JINC,EQ,-1)JJ=J
      IF(JINC,AFUN(JJ),LE,1.0E-10)GO TO 660
      X1=AFUN(JJ)*(XL(J,I)-XL(JOLD,I))
      IF(X1,LE,3.0)GO TO 630
      IF(IPASS,LE,NFORCE)GO TO 620

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600 IF(LNCT,LT,NPAGE)GO TO 600
WRITE(LOG2,500)
LNCT=1
LNCT=LNCT+1
WRITE(LOG2,610)IPASS,I,ITER,JJ,X1
FORMAT(5X,4HPASS,I3,9H STATION,I3,11H ITERATION,I3,12H STREAMTU
15E,I3,43H MOME,1F4 EQUATION EXPONENT ABOVE LIMIT AT,E13.5)
IFAIL=1
X1=84.0
X1=EXP(X1)
VV(J)=VV(JOLD)*X1+(1.0-X1)*BFUN(JJ)/AFUN(JJ)
IF(J,EO,K)GO TO 670
IF(J,EO,NSTR4S)GO TO 650
GO TO 590
J=IMIU
JINC=-1
GU TO 590
VV(J)=VV(JOLD)+BFUN(JJ)*(XL(J,I)-XL(JOLD,I))
GO TO 640
GO 710 J=K,NSTRMS
IF(VV(J).LE.4.0*VVOLD(IMID)**2)GO TO 676
IF(IPASS,LE,NFORCE)GO TO 674
CALL UD0303(LNCT,I)
WRITE(LOG2,672)IPASS,I,ITER,J
FORMAT(5X,4HPASS,I3,9H STATION,I3,11H ITERATION,I3,12H STREAMLI
1NE,I3,50H MERIDIONAL VELOCITY,3GREATER THAN TWICE MID VALUE)
VV(J)=4.0*VVOLD(IMID)**2
IF(VV(J).GE.1.0)GO TO 702
IF(IPASS,LE,NFORCE)GO TO 700
IF(LNCT,LT,NPAGE)GO TO 630
WRITE(LOG2,500)
LNCT=1
LNCT=LNCT+1
WRITE(LOG2,630)IPASS,I,ITER,J,VV(J)
FORMAT(5X,4HPASS,I3,9H STATION,I3,11H ITERATION,I3,12H STREAMLI
1NE,I3,40H MERIDIONAL VELOCITY,3SQUARED BELOW LIMIT AT,E13.5)
VV(J)=1.0
IFAIL=1
GO TO 710
VV(J)=SQRT(VV(J))
IF(VV(J).LE.VMAX(J))GO TO 710
IFAIL=1
IF(IPASS,LE,NFORCE)GO TO 708
CALL UD0303(LNCT,I)
WRITE(LOG2,706)IPASS,I,ITER,J,VV(J),VMAX(J)
FORMAT(5X,4HPASS,I3,9H STATION,I3,11H ITERATION,I3,12H STREAMLI
1NE,I3,44H MERIDIONAL VELOCITY ABOVE SOUND SPEED VM=F8.2,3H A=F
28.2)
VV(J)=VMAX(J)

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710 CONTINUE
711 X1=0.0
712 J=K,IFUE
713 X1=X1+(XL(J+1,I)-XL(J,I))*ATS((VV(J+1)+VV(J))/(VVJLJ(J+1)+VVOLD(J)
1)-1.0)
714 X1=X1/(XL(NSI+MS,I)-XL(K,I))
715 X2=0.1
716 IF(X1,LT,(.2)*X2=EXP(-11.52*X1)
717 J=K,NSI+MS
718 VV(J)=VVOLD(J)+X2*(VV(J)-VVOLD(J))
719 IF(MLOS(I).EQ.1.AND.VL2(I).EQ.J)CALL UD9307
720 J=1,IFUR
721 HS(J)=(H(J,I)+H(J+1,I))/2.0-((VV(J)+VV(J+1))/2.0)**2+((VM(J,I)+VM
1(J+1,I))/2.0)**2/(2.0*G+J)
722 IF(HS(J).GE.HMIN)GO TO 800
723 IF(IPASS.LE.NPAGE)GO TO 790
724 IF(LT.LT.NPAGE)GO TO 770
725 WRITE(LUG2,530)
726 LNCI=1
727 LNCI=LNCI+1
728 WRITE(LUG2,730)IPASS,I,ITER,J,HS(J)
729 FORMAT(2X,4HPASS,I3,3H STATION,I3,11H ITERATION,I3,12H STR=AMTUS
13E,I3,53H STATIC ENTHALPY BELOW LIMIT IN CONTINUITY EQUATION AT,E
213.5)
730 IF(FAIL=1)
731 HS(J)=HMIN
732 XM2(J)=UDG9(HS(J),S(J,I)+S(J+1,I))/2.0,((VV(J)+VV(J+1))/2.0)**2)
733 GO TO 1100
734 J=IMID
735 JINC=1
736 LOOP=1
737 JOLD=J
738 J=J+JINC
739 IF(JINC.EQ.-1)JJ=J
740 VOLD=VV(J)
741 VAV=(VOLD+VV(JOLD))/2.0
742 IF(FAIL=0)
743 ICONF2=0
744 X2=(TBETA(J,I)+TBETA(JOLD,I))/2.0
745 X1=(XI(J)+XI(JOLD))/2.0+(XN*(R(J,I)+P(JOLD,I))/2.0)**2-VAV**2*(1.
1)+X2*X2)/(2.0*G+J)
746 IF(X1,GE.HMIN)GO TO 870
747 IF(IPASS.LE.NPAGE)GO TO 860
748 IF(LT.LT.NPAGE)GO TO 840
749 WRITE(LUG2,530)
750 LNCI=LNCI+1
751 WRITE(LUG2,830)IPASS,I,ITER,J,JOLD,X1
752 FORMAT(2X,4HPASS,I3,3H STATION,I3,11H ITERATION,I3,12H STREA:TU

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135, I3, PH LOOP, I3, +3H STATIC H IN MOMENTUM EQUIN. BELOW LIMIT AT, E
213.5)
IF AIE=1
IFCONF2=1
X1=HMIN
X3=(S(J,I)+S(JOLD,I))/2.0
XP=UDG8(X1,X3)
X7=UDG7(X1,X3)
X1=UDG9(X1,X3,VAV*VAV)
IF(X1.LE.0.9301)GO TO 910
IF(IPASS.LE.4FORCE)GO TO 900
IF(LNCT.LT.NPAGE)GO TO 880
WRITE(LOG2,500)
LNCT=1
LNCT=LNCT+1
X1=SQRT(X1)
WRITE(LOG2,600)IPASS,I,ITER,JJ,LOOP,X1
FORMATT(5X,4H PASS, I3, 3H STATION, I3, 11H ITERATION, I3, 12H STREAMTU
185, I3, 6H LOOP, I3, 39H MERIDIONAL MACH NUMBER ABOVE LIMIT AT, E13.5
2)
IF AIE=1
IFCONF2=1
X1=0.9501
X4=(SPG(J)+SPG(JOLD))/2.0
X5=(CPG(J)+CPG(JOLD))/2.0
X9=(R(J,I)+R(JOLD,I))*0.5
X10=SIN((PHI(J)+PHI(JOLD))*0.5)
X11=(1.0-X5*X1)*(CR(J)+CR(JOLD))*0.5/XP+X9/VAV**2+(DLADM(J)+DLADM(JOLD))/(LAMI(J)+LA
1J/X9*(1.0+X1*(X2+X4*X9/VAV)**2)
2MI(JOLD))
CV2DL=FX2(JJ)-X7*DSDL(JJ)-2.0*X1*VAV*X2*GUS((GAMA(J)+GAMA(JOLD))*J
1.0)+VAV*VAV*(X11/(1.0-X1)-FX1(JJ))
X12=1.0/(1.0+X2*X2)
QVMDVM(JJ)=X12*(X7*DSDL(JJ)-FX2(JJ))/VAV**2-FX1(JJ)+X11/(1.0-X1))
IF(I.EQ.1)CR.I.EQ.NSTNS.OR.IPASS.EQ.1)GO TO 920
IF(NEGN.EQ.1)GO TO 914
X8=(TANEPS(J)+TANEPS(JOLD))*0.5
X5=0.5*(OSUM(J)+OSUM(JOLD))*X7*(X4*(X12+X6*X1/(1.0-X1))-X8*X2*X12)
CV2DL=UV2DL+X5-VAV*(ORVWDM(J)+ORVWDM(JOLD))*0.5*(X8-X4*X1*X2/(1.0-
1X1))
QVMDVM(JJ)=QVMDVM(JJ)-X5*X12/VAV**2
GO TO 920
X5=0.5*(OSUM(J)+OSUM(JOLD))*X7*X4*(1.0-X1*(X6-1.0))/(1.0-X1)
QV2DL=QV2DL+X5
QVMDVM(JJ)=QVMDVM(JJ)-X5*X12/VAV**2
QV2DL=QV2DL+2.0*X12
X1=VV(JOLD)**2+QV2DL*(XL(J,I)-XL(JOLD,I))
IF(X1.LE.9.0*VVJOLD(IMID)**2)GO TO 938
IFCONF2=1
IF AIE=1

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1010 JINC=-1
1011 GO TO 820
1012 IF (I.EQ.1) GO TO 1014
1013 IF (NLOSS(I).EQ.2.0R.(NLOSS(I).EQ.1.AND.NL2(I).EQ.0)) CALL UD0307
1014 GO 1090 J=1, ITUB
1015 X1=((V(V(J)+V(V(J+1)))/2.0)**2*(1.0+((TBETA(J,I)+TBETA(J+1,I))/(2.0)**
1016 12)
1017 HS(J)=(X1(J)+X1(J+1))/2.0+((XV*(R(J,I)+R(J+1,I))/(2.0)**2-X1)/(2.0*
1018 1G*EJ)
1019 IF (HS(J).GE.HMIN) GO TO 1080
1020 IF (IPASS.LE.NFORCL) GO TO 1070
1021 IF (LNCT.LT.NPAGE) GO TO 1050
1022 WRITE (LOG2,500)
1023 LNCT=1
1024 LNCT=LNCT+1
1025 WRITE (LOG2,730) IPASS,I,ITER,J,HS(J)
1026 IF (FAIL=1)
1027 HS(J)=HMIN
1028 XM2(J)=UDG4(HS(J),S(J,I)+S(J+1,I))/2.0,X1)
1029 IF (I.EQ.1.0R.NLOSS(I).NE.1.0R.NL2(I).NE.0) GO TO 1090
1030 X1=(S(J,I)+S(J+1,I))/2.0
1031 X2=UDG4(HS(J),X1)
1032 X3=(X1(J)+X1(J+1))/2.0+(XN*(R(J,I)+R(J+1,I))/(2.0)**2/(2.0*G*EJ)
1033 X3=UDG4(X3,X1)
1034 XM2(J)=XM2(J)*(1.0+X*(LOSS(J)+LOSS(J+1))/2.0*X2/(X3*(1.0+(LOSS(J)
1035 1+LOSS(J+1))/2.0*(1.0-X2/X3)))
1036 1 CONTINUE
1037 DELW(1)=0.0
1038 CWDUV=0.0
1039 X2=RRLOCK(I)*RDIST(I)
1040 X3=RRLOCK(I)*(1.0-3DIST(I))*2.0/XL(NSTRMS,I)
1041 GO 1200 J=1, ITUB
1042 X1=DL(J)*(R(J,I)+R(J+1,I)+UDG5(HS(J),S(J,I)+S(J+1,I))/2.0)*(V(V(J)
1043 1)+V(V(J+1)))*(COPG(J)+COPG(J+1))*PI/(4.0*SCLFAC**2)
1044 X1=X1*(LAMI(J)+LAMI(J+1))/2.0-WWBL(I)-X2-X3*(XL(J,I)+XL(J+1,I))
1045 CELW(J+1)=CELW(J)+X1
1046 XT=0.0
1047 IF (J.GE.IMIO) GO TO 1130
1048 L1=J
1049 X4=X4+DVMCVML1)
1050 IF (L1.GE.IMIJ-1) GO TO 1120
1051 L1=L1+1
1052 GO TO 1110
1053 X4=X4/FLOAT(IMIO-J)
1054 GO TO 1200
1055 L1=IMIO+1
1056 X4=X4+DVMCVML1)
1057 IF (L1.GE.IMIJ) GO TO 1150
1058 L1=L1+1

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1150 GO TO 1140
1200 X4=X4/FLD*AT(J-IMID+1)
      DMV=DMV+X1*(1.0-VM2(J))*2.0/((VV(J)+VV(J+1))*(1.0-((XL(J,I)+XL(J
      +1,I))*0.5-XL(IMID,I))*X4))
      VM2=DMV/WM*VV(IMID)
      DELW(J)=DELW(J)/WM TO 1250
      IF(DMV.LE.U.U)GO TO 1330
      IF(NMACH(I).EQ.1)GO TO 1330
      IF(W.LT.FLOW(ICASE).AND.ICONF1.EQ.0)VMAX=VV(IMID)
      CV=(FLOW(ICASE)-W)/DMV
      IF(CV.LT.-0.1*VV(IMID))UV=-0.1*VV(IMID)
      IF(IPASS.EU.1.OR.(I.NE.1.AND.NWORK(I).LE.4))GO TO 1234
      IF(VV(IMID)+CV.LT.VMIN)GO TO 1232
      CV=(VMIN-VV(IMID))*0.5
      IF(VV(IMID)+CV.GT.VMAX)GO TO 1234
      DO 1270 J=K,NSTRMS
      VV(J)=VV(J)+CV
      IF(VV(J).LE.VMAX(J))GO TO 1238
      IF(FAIL=1)
      VV(J)=VMAX(J)
      IF(VV(J).GE.1.0)GO TO 1270
      IF(IPASS.LE.NPAGE)GO TO 1240
      WRITE(LOG2,500)
      LNCT=LNCT+1
      WRITE(LOG2,1250)IPASS,I,ITER,J,VV(J)
      FORMAT(5X,'HPASS,I3.9H STATION,I3.11H ITERATION,I3.12H
      NE,I3.50H MERIDIONAL VELOCITY BELOW LIMIT IN CONTINUITY AT,E13.5)
      VV(J)=1.0
      IF(FAIL=1)
      CONYINUE
      GO TO 1340
      IF(NMACH(I).EQ.0)GO TO 1290
      IF(W.LT.FLOW(ICASE).AND.ICONF1.EQ.0)VMIN=VV(IMID)
      GO TO 1220
      IF(VV(IMID).LT.VMIN.AND.ICONF1.EQ.0)VMIN=VV(IMID)
      CV=-0.1*VV(IMID)
      IF(FAIL=1)
      IF(IPASS.LE.NPAGE)GO TO 1310
      IF(LNCT.LT.NPAGE)GO TO 1310
      WRITE(LOG2,500)
      LNCT=LNCT+1
      WRITE(LOG2,1320)IPASS,I,ITER
      FORMAT(5X,'HPASS,I3.9H STATION,I3.11H ITERATION,I3.43H OTHER CO

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1330      INFINITY (EQUATION BRANCH REQUIRED)
      GO TO 1230
      IF (V(I,IMIN).GT.VMAX.AND.ICONF1.EQ.0)VMAX=V(I,MID)
      QV=0.1*V(I,IMID)
      GO TO 1300
1340      X1=TOLNCE/5.
      IF (NEVAL(I).GT.0)X1=X1/2.0
      IF (ABS(W/FLOW(ICASE))-1.0).GT.X1)GO TO 1354
      DO 1350 J=X,NSTRMS
      IF (ABS(V(I,J)/VVOLD(J)-1.0).GT.X1)GO TO 1354
      CONTINUE
1350      GO TO 1330
1354      IF (I.EQ.1)GO TO 1360
      IF (I.EQ.1)GO TO 400
      IF (NL2(I).EQ.1.AND.NL2(I).EQ.0).OR.(NWORK(I).GE.5.AND.NLOSS(I).
1      EQ.2))CALL UD0307
      GO TO 400
1360      IF (IPASS.LE.NFORCE)GO TO 1390
      IF (LNCT.LT.NPAGE)GO TO 1370
      WRITE(LOG2,500)
      LNCT=1
      LNCT=LNCT+1
      X1=W/FLOW(ICASE)
      X2=V(I,IMIN)/VVOLD(K)
      X3=V(I,IMIN)/VVOLD(I,MID)
      X4=V(I,IMIN)/VVOLD(NSTRMS)
      WRITE(LOG2,1330)IPASS,I,X1,X2,X3,X4
      FORMAT(5X,H=ASS,I3.9H STATION,I3.49H MOMENTUM AND/OR CONTINUITY
1      UNCONVERGED W/WSPEC=F9.5,16H VM/VW(OLD) HU3=F8.5,5H MID=F8.5,5
2      H T F8.2)
      IF (IFAIL.NE.J.AND. IFAIL0.EQ.0)IFAIL0=I
      GO 1400 J=1,NSTRMS
      VM(I,I)=V(I,J)
      IF (I.NE.1)GO TO 1420
      DO 1410 J=1,NSTRMS
      VM(J,1)=V(I,J)*TETA(J,1)
      GO TO 1440
      IF (NMX.NE.1)GO TO 1440
      DO 1430 J=1,NSTRMS
      S(J,I-1)=SKEEP(J)
      VM(J,I-1)=HKEEP(J)
      IF (NWORK(I).GE.5)GO TO 1460
      TETA(1,I)=0.0
      DO 1450 J=K,NSTRMS
      TETA(J,I)=VM(J,I)-XN*(J,I)/V(I,J)
      GO TO 1480
      DO 1470 J=1,NSTRMS
      VM(J,I)=V(I,J)+XN*(J,I)
      H(J,I)=X1(J)+XN*(J,I)/(G+EJ)

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1480 CONTINUE
END

3083 602
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160      XI(J)=XL(J,I+1)/XL(NSTRMS,I+1)
161      LI=IS2(I+1)
162      CALL UD0301(JATAC(L1),DATA4(L1),NDATA(I+1),XX1,XX1,X1,NSTRMS,NTE,RP
163      1(I+1),0)
164      GO TO 200 J=1,NSTRMS
165      LAM IPI(J)=1.-XX1(J)
166      GO TO 230 J=1,NSTRMS
167      X1=SQRT((X(J,I+1)-X(J,I))**2+(X(J,I+1)-X(J,I))**2)
168      X2=SQRT((X(J,I+1)-X(J,I))**2+(X(J,I+1)-X(J,I))**2)
169      X3=ATAN2(X(J,I+1)-X(J,I),X(J,I+1)-X(J,I))
170      X4=ATAN2(X(J,I+1)-X(J,I),X(J,I+1)-X(J,I))
171      PHI(J)=(X3+X4)/2.0
172      CR(J)=(X3-X4)/(X1+X2)*2.0
173      CSDM(J)=0.0
174      CRVMDM(J)=0.0
175      IF(IIPASS.EG.1)GO TO 220
176      IF(IIPASS.EG.1)GO TO 220
177      CSDM(J)=((S(J,I+1)-S(J,I))/X1+(S(J,I)-S(J,I-1))/X2)/2.0*GEJ
178      CRVMDM(J)=((R(J,I+1)-R(J,I))*VM(J,I)+VM(J,I)*VM(J,I)-
179      1RIM1(J)*VM(J,I-1))/X2/(2.0*P(J,I))
180      CSDM(J)=((V4(J,I+1)-VM(J,I))/X1+(VM(J,I)-VM(J,I-1))/X2)*0.5
181      CRVMDM(J)=((V4(J,I+1)-VM(J,I))/X1+(VM(J,I)-VM(J,I-1))/X2)*0.5
182      IF(IIPASS.EG.1)GO TO 220
183      IF(IIPASS.EG.1)GO TO 220
184      CRK(I+1)=EG(J)GO TO 340
185      LI=NO1MEM(I)+1
186      GO TO 221,223,225,227),L1
187      GO TO 221 J=1,NSTRMS
188      TE IPI(J)=R(J,I)
189      GO TO 224 J=1,NSTRMS
190      TE IPI(J)=R(J,I)/R(NSTRMS,I)
191      GO TO 223
192      GO TO 226 J=1,NSTRMS
193      TE IPI(J)=XL(J,I)
194      GO TO 229
195      GO TO 228 J=1,NSTRMS
196      TE IPI(J)=XL(J,I)/XL(NSTRMS,I)
197      LI=IS2(I)
198      CALL UD0301(JATAC(L1),DATA3(L1),NDATA(I),TEIPI,TEIPI,X1,NSTRMS,NTE
199      1RP(I),0)
200      X1=SP2E(J,I+1)*SQFAC(ICASE)*PI/(30.0*SCLFAC)
201      GO TO 230 J=1,NSTRMS
202      TE IPI(J)=IAN(TEIPI(J)/C1)
203      TE IPI(J)=(VM(J,I)-X1*R(J,I))/VM(J,I)
204      GO TO 330
205      GO TO 240 J=1,NSTRMS
206      CSDM(J)=0.0
207      CRVMDM(J)=0.0
208      CR(J)=0.0
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246 IF(I,50,1)GO TO 244
246 PHI(J)=ATAN2(R(J,I)-RIM1(J),X(J,I)-XIM1(J))
244 GO TO 390
260 PHI(J)=ATAN2(R(J,2)-R(J,1),X(J,2)-X(J,1))
260 XI(J)=H(J,1)
270 LAMIP1(J)=1.0
270 IF(NDATA(2).EQ.0)GO TO 390
270 L2=NDIMEN(2)+1
290 GO TO(250,310,330,350),L2
300 GO 300 J=1,NSTRMS
300 XX1(J)=R(J,2)
310 GO TO 370
320 J=1,NSTRMS
320 XX1(J)=R(J,2)/R(NSTRMS,2)
330 GO TO 370
340 J=1,NSTRMS
340 XX1(J)=XL(J,2)
350 GO 350 J=1,NSTRMS
350 XX1(J)=XL(J,2)/XL(NSTRMS,2)
360 L1=ISG(2)
370 CALL U003C1(JATAC(L1),DATA4(L1),NDATA(2),XX1,XX1,X1,NSTRMS,INTERP(2),
1,0)
380 J=1,NSTRMS
380 LAMIP1(J)=1.0-XV1(J)
380 CALL U00301(R(1,I),X(1,I),NSTRMS,R(1,I),X1,GAMA,NSTRMS,0,1)
390 GAMA(J)=ATAN(GAMA(J))
390 SPFG(J)=GAMA(J)+CHI(J)
390 SPFG(J)=COS(SPFG(J))
400 SPFG(J)=SIN(SPFG(J))
400 VV(J)=VM(J,I)
400 VV(J)=V(I,I)-XL(J,I)
410 OSUL(J)=XL(J,I)*G*EJ/DL(J)
410 IF(I,50,1,OR,WORK(I).GE.5)GO TO 430
420 DVMVM(J)=0.0
420 FX1(J)=(VM(J,I))/(R(J+1,I)+R(J,I))*(R(J+1,I)*VM(J+1,I)-R
1FX2(J)=(H(J+1,I)-H(J,I))/DL(J)*G*EJ
430 GO TO 450
430 FX1(J)=(TETA(J+1,I)+TETA(J,I))/(R(J+1,I)+R(J,I))*(R(J+1,I)*TETA
1FX2(J)=(XI(J+1,I)-XI(J))/DL(J)*G*EJ
440

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JJ=JOLD
EQ=-1)JJ=J
IF(ABS(AFUN(JJ)).LE.1.0E-10)GO TO 660
X1=-AFUN(JJ)*(XL(J,I)-XL(JOLD,I))
IF(ABS(X1).LE.1.0E-10)GO TO 600
IF(X1.LE.83.3)GO TO 630
IF(IPASS.LC.NFORC)GO TO 520
IF(LNCT.LT.NPAGE)GO TO 500
WRITE(LOG2,500)
LNCT=LNCT+1
WRITE(LOG2,610)IPASS,I,ITER,JJ,X1
FORMAT(3X,4HBPASS,I3,11H STATION,I3,11H ITERATION,I3,12H STREAMLINE
,I3,11H MOMENTUM EQUATION EXPONENT ABOVE LIMIT AT,E13.5)
IFAIL=1
X1=84.0
X1=EXP(X1)
VV(J)=VV(JOLD)*X1+(1.0-X1)*3FUN(JJ)/AFUN(JJ)
IF(J.EQ.0.K)GO TO 570
IF(J.EQ.NSTRMS)GO TO 550
GO TO 590
J=IMID
JINCE=-1
GO TO 590
VV(J)=VV(JOLD)+3FUN(JJ)*(XL(J,I)-XL(JOLD,I))
GO TO 600
GO 710 J=K.NSTRMS
IF(VV(J).LE.+0.0*VVOLD(IMID))*2)GO TO 676
IF(IPASS.LE.NFORC)GO TO 674
CALL UD0303(LNCT,1)
WRITE(LOG2,672)IPASS,I,ITER,J
FORMAT(3X,4HBPASS,I3,11H STATION,I3,11H ITERATION,I3,12H STREAMLINE
,I3,11H MERIDIONAL VELOCITY GREATER THAN TWICE MID VALUE)
1NZ,I3,50H*VVOLD(IMID)*+2
VV(J)=+0.0*VVOLD(IMID)GO TO 702
IF(VV(J).GE.+1.0)GO TO 700
IF(IPASS.LE.NFORC)GO TO 680
IF(LNCT.LT.NPAGE)GO TO 500
WRITE(LOG2,500)
LNCT=LNCT+1
WRITE(LOG2,630)IPASS,I,ITER,J,VV(J)
FORMAT(3X,4HBPASS,I3,11H STATION,I3,11H ITERATION,I3,12H STREAMLINE
,I3,11H MERIDIONAL VELOCITY SQUARED BELOW LIMIT AT,E13.5)
1NE,I3,46H
VV(J)=1.0
IFAIL=1
GO TO 710
VV(J)=SQRT(VV(J))
X1=0.0

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712      GO 712 J=K, I, IUB
      X1=X1+(XL(J+1,I)-XL(J,I))*ABS((VV(J+1)+VV(J))/(VVOLD(J+1)+VVOLD(J)
1) -1.0)
      X1=X1/(XL(NS TRMS,I)-XL(K,I))
      IF(X1.LT.0.2)X2=X1*(-11.52*X1)
      GO 715 J=K, NS1PMS
      VV(J)=VVOLD(J)+X2*(VV(J)-VVOLD(J))
      IF(NLOC2(I).EQ.1)X2=X1*10.0*U2(I).E2.J)CALL UC0307
      GO 800 J=1, I, IUB
      HS(J)=(H(J,I)+H(J+1,I))/2.0-((VV(J)+VV(J+1))/2.0)**2+((VV(J,I)+VV
1(J+1,I))/2.0)**2/(2.0*G*EJ)
      IF(HS(J).GE.HMIN)GO TO 800
      IF(IPASS.LE.NFORCE)GO TO 770
      IF(LNCT.LT.NPAGE)GO TO 770
      WRITE(LUG2,5JJ)
      LNCT=LNCT+1
      WRITE(LUG2,7JJ)IPASS,I,ITER,J,HS(J)
      FORMAT(5X,'4HPASS',I3.9H 'STATION',I3.11H 'ITERATION',I3.12H 'STRENGTH'
12E,13.5)
      IF(LIL=1)
213.5)
      HS(J)=HMIN
      XM2(J)=UDG9(HS(J),(S(J,I)+S(J+1,I))/2.0,((VV(J)+VV(J+1))/2.0)**2)
      GO TO 1100
      J=IMIU
      JINCE=1
      LOOP=1
      JOLD=J
      J=J+JINC
      J=JOLD
      IF(JINC.EQ.-1)JJ=J
      VOLD=VV(J)
      VAV=(VOLD+VV(JOLD))/2.0
      IF(FAIF.EQ.
      LCONF2=0
      X2=(TBETA(J,I)+TBETA(JOLD,I))/2.0
      X1=(X1(J)+X1(JOLD))/2.0+((XN*(R(J,I)+R(JOLD,I))/2.0)**2-VAV**2*(1.
10+X2*X2))/(2.0+3*JJ)
      IF(X1.GE.HMIN)GO TO 870
      IF(IPASS.LE.NFORCE)GO TO 860
      IF(LNCT.LT.NPAGE)GO TO 840
      WRITE(LUG2,5JJ)
      LNCT=LNCT+1
      WRITE(LUG2,7JJ)IPASS,I,ITER,JJ,LOOP,X1
      FORMAT(5X,'4HPASS',I3.9H 'STATION',I3.11H 'ITERATION',I3.12H 'STRENGTH'
12E,13.5)
      IF(LIL=1)
213.5)

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860 IFAIE=1
870 IFCONF2=1
      X3=(S(J,I)+S(JOLD,I))/2.0
      X7=UDG7(X1,X3)
      X4=(SPPG(J)+SPPG(JOLD))*0.5
      X5=(CPPG(J)+CPPG(JOLD))*0.5
      X1=X5*(CR(J)+CR(JOLD))*0.5-FX1(JJ)
      X12=1.0+X2*X2
      X8=(TANES(J)+TANESPS(JOLD))*0.5
      X11=FX2(JJ)-X7*CSUL(JJ)
      X6=X4*(DVM(J)+DVM(JOLD))*0.5-2.0*XM*X2*COS((GAMA(J)+GAMA(JOLD)
1) *0.5)
      IF(IPASS.EQ.1.OR.I.EQ.1.0R.I.EQ.NSTNS)GO TO 920
      IF(NEQN.EQ.3)GO TO 900
      X11=X11+X7*(DSO1(J)+DSO1(JOLD))*0.5*(X4*X12-X8*X2*X12)
      X6=X6-X3*(DRVWDM(J)+DRVWDM(JOLD))*0.5
      GO TO 920
      X11=X11+X7*(DSO1(J)+DSO1(JOLD))*0.5*X4
      DVM2DL=2.0*(VAV*(X6+VAV*X1)+X11)
      DVM2DVM(JJ)=X12*(X1-VAV**2)
      X1=VV(JOLD)**2+DV2DL*(XL(J,I)-XL(JOLD,I))
      IF(X1.LE.0.0*VVOLD(IMID)**2)GO TO 938
      IFCONF2=1
      IF(IPASS.LE.NFORCE)GO TO 936
      CALL UD0303(LNCT,1)
      X1=SQRT(X1)
      X2=3.0*VVOLD(IMID)
      WRITE(LOG2,933)IPASS,I,ITER,J,LOOP,X1,X2
      FORMAT(5X,4HPASS,I3,9H ITERATION,I3,12H STREAMLI
1NE,I3,6H LOOP,I3,33H MERIDIONAL VELOCITY ABOVE LIMIT,E13.5,9H L
2NE,I3,6H LOOP,I3,33H MERIDIONAL VELOCITY ABOVE LIMIT,E13.5,9H L
      X1=9.0*VVOLD(IMID)**2
      IF(X1.GE.1.0)GO TO 950
      IF(IPASS.LE.NFORCE)GO TO 944
      IF(LNCT.LT.NPAGE)GO TO 330
      WRITE(LOG2,900)
      LNCT=LNCT+1
      WRITE(LOG2,940)IPASS,I,ITER,J,LOOP,X1
      FORMAT(5X,4HPASS,I3,9H ITERATION,I3,11H
1NE,I3,6H LOOP,I3,46H (MERIDIONAL VELOCITY) SQUARED BELOW LIMIT A
2NE,I3,5)
      IF(I.EQ.1)
      IFCONF2=1
      VV(J)=SQRT(X1)
      IF(ABS(VV(J)/VOLD-1.0).LE.TOLNCE/5.0)GO TO 990
      IF(LOOP.GE.L*MAX)GO TO 960

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[illegible]

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1110      GO 1200 J=1, IUT
1111      XI=OL(J)*(P(J+1,I)+R(J,I))*UUGS(HS(J),(S(J,I)+S(J+1,I))/2.0)*(VV(J
1112      1)+VV(J+1,I))*COPG(J)+COPG(J+1))*I/(4.0*SCLFAC**2)
1113      XI=XI*(LAM(I(J))+LAM(I(J+1)))/2.0-WMBL(I)-X2-X3*(XL(J,I)+XL(J+1,I))
1114      CELW(J+1)=DELTA(J)*XI
1115      X4=0.0
1116      IF(J.GE.IMID)GO TO 1130
1117      L1=J
1118      X4=X4+DVMQVM(L1)
1119      IF(L1.GE.IMI)-1)GO TO 1120
1120      L1=L1+1
1121      GO TO 1110
1122      X4=X4/FLOAT(I4I7-J)
1123      GO TO 1200
1124      L1=IMID+1
1125      X4=X4+DVMQVM(L1)
1126      IF(L1.GE.J)GO TO 1150
1127      L1=L1+1
1128      GO TO 1110
1129      X4=X4/FLOAT(J-IMID+1)
1130      DMCV=DMDV+X1*(1.0-X42(J))*2.0/((VV(J)+VV(J+1))*(1.0-(XL(J,I)+XL(J
1131      1+1,I))*0.5-XL(IMI,I))*X4)
1132      W=DELMW(NSRMS)
1133      FM2=DMDV/W+VV(IMI)
1134      CELW(J)=DELW(J)/W
1135      IF(DMDV.LE.0.0)GO TO 1250
1136      IF(NMAC(I)).EQ.1)GO TO 1330
1137      IF(W.LE.FLOW(ICASE)-W)/DMDV
1138      DV=(DV.LF.-0.1*VV(I4I))DV=-0.1*VV(IMI)
1139      IF(DV.GT.0.1*VV(I4I))DV=0.1*VV(IMI)
1140      IF(IPASS.EQ.1)CR(I,NE,1)AND.WORK(I).LE.4))GO TO 1234
1141      IF(VV(IMI)+DV.LI.VMIN)GO TO 1232
1142      DV=(VMIN-VV(IMI))*0.5
1143      IF(VV(IMI)+DV.GT.VMAX)GO TO 1234
1144      DV=(VMAX-VV(IMI))*0.5
1145      GO 1270 J=K,NSTRMS
1146      VV(J)=VV(J)+V
1147      IF(VV(J).GE.1.0)GO TO 1270
1148      IF(IPASS.LE.NFURCE)GO TO 1260
1149      IF(LNCT.LI.NPAGE)GO TO 1240
1150      WRITE(LOG2,5JJ)
1151      LNCT=1
1152      LNCT=LNCT+1
1153      WRITE(LOG2,4)HPASS,I3,9H STATION,I3,11H ITERATION,I3,12H STREAMLI
1154      FORMAT(5X,4H PERIODICAL VELOCITY BELOW LIMIT IN CONTINUITY A1,E13.5)
1155      INE,I3,50H
1156      VV(J)=1.0
1157      IFAIL=1

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1270 CONTINUE
1280 GO TO 1340
1290 IF (NMACH(I).EQ.0) GO TO 1290
1300 IF (W/LT.FLOW(ICASE).AND.ICONF1.EQ.0) VMIN=VV(IMID)
1310 GO TO 1220
1320 IF (VV(I410).LT.VMIN.AND.ICOUF1.EQ.0) VMIN=VV(IMID)
1330 QV=-.1+VV(IMI)
1340 IF (IPL=1) LE=VFCO2) GO TO 1230
1350 IF (IPL=1) LE=VFCO2) GO TO 1310
1360 WRITE(LU62,500)
1370 LNCT=LNCT+1
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1410 VW(J,1)=VV(J)*TBETA(J,1)
1420 GO TO 1440
1430 IF (MIX.NE.1) GO TO 1440
1440 J=1,NSTRMS
1450 H(J,I-1)=SKEEP(J)
1460 VW(J,I-1)=VWKEP(J)
1470 IF (NWK(I).GE.5) GO TO 1460
1480 TBETA(1,I)=0.0
1490 TBETA(J,I)=(VW(J,I)-XN*R(J,I))/VV(J)
1500 GO TO 1480
1510 J=1,NSTRMS
1520 VW(J,I)=VV(J)*TBETA(J,I)+XN*R(J,I)
1530 H(J,I)=XI(J)+XN*R(J,I)/(G*EJ)
1540 CONTINUE
1550 END

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[illegible]

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170 READ (LOG1,130) (XSTA(K,I),PSTA(K,I),K=L,KPT)
180 IF (KPTS(I).G-.2) GO TO 170
190 XPTS(I)=XSTA(1,I)
200 XSTA(2,I)=XSTA(1,I)+1.0
210 READ (LOG1,130) (P(I,J),BLAFOR(I,J),J=1,NLINES)
220 FORMAT (2I3)
230 IDUM=KPTS(I)
240 IF (NLINES.GT.IDUM) IDUM=NLINES
250 WRITE (LOG2,200)
260 FORMAT (1H1)
270 LNC1=LNC1+IDUM+7
280 IF (LNC1.NE.0) GO TO 240
290 WRITE (LOG2,220) I,KPTS(I),I,IFANGS(I)
300 FORMAT (2X,I3,10X,7HCOMPUTING STATION,I3,5X,28HNUMBER OF DESCRIPTION,9X,10HSTR
310 POINTS,I3,5X,7HIFANGS(I2,2H)=,I3,76X,11HDESCRIPTION,9X,10HSTR
320 LINE,K=1,100
330 IF (K.LE.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
340 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
350 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
360 CONTINUE
370 IF (LNC1.EQ.0) GO TO 300
380 IF (LNC1.GT.0) GO TO 300
390 IF (LNC1.EQ.1) GO TO 300
400 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
410 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
420 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
430 CONTINUE
440 IF (LNC1.EQ.0) GO TO 300
450 IF (LNC1.GT.0) GO TO 300
460 IF (LNC1.EQ.1) GO TO 300
470 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
480 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
490 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
500 CONTINUE
510 IF (LNC1.EQ.0) GO TO 300
520 IF (LNC1.GT.0) GO TO 300
530 IF (LNC1.EQ.1) GO TO 300
540 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
550 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
560 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
570 CONTINUE
580 IF (LNC1.EQ.0) GO TO 300
590 IF (LNC1.GT.0) GO TO 300
600 IF (LNC1.EQ.1) GO TO 300
610 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
620 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
630 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
640 CONTINUE
650 IF (LNC1.EQ.0) GO TO 300
660 IF (LNC1.GT.0) GO TO 300
670 IF (LNC1.EQ.1) GO TO 300
680 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
690 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
700 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
710 CONTINUE
720 IF (LNC1.EQ.0) GO TO 300
730 IF (LNC1.GT.0) GO TO 300
740 IF (LNC1.EQ.1) GO TO 300
750 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
760 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
770 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
780 CONTINUE
790 IF (LNC1.EQ.0) GO TO 300
800 IF (LNC1.GT.0) GO TO 300
810 IF (LNC1.EQ.1) GO TO 300
820 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
830 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
840 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
850 CONTINUE
860 IF (LNC1.EQ.0) GO TO 300
870 IF (LNC1.GT.0) GO TO 300
880 IF (LNC1.EQ.1) GO TO 300
890 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
900 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
910 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
920 CONTINUE
930 IF (LNC1.EQ.0) GO TO 300
940 IF (LNC1.GT.0) GO TO 300
950 IF (LNC1.EQ.1) GO TO 300
960 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
970 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
980 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
990 CONTINUE
1000 IF (LNC1.EQ.0) GO TO 300
1010 IF (LNC1.GT.0) GO TO 300
1020 IF (LNC1.EQ.1) GO TO 300
1030 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
1040 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
1050 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
1060 CONTINUE
1070 IF (LNC1.EQ.0) GO TO 300
1080 IF (LNC1.GT.0) GO TO 300
1090 IF (LNC1.EQ.1) GO TO 300
1100 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
1110 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
1120 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
1130 CONTINUE
1140 IF (LNC1.EQ.0) GO TO 300
1150 IF (LNC1.GT.0) GO TO 300
1160 IF (LNC1.EQ.1) GO TO 300
1170 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
1180 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
1190 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
1200 CONTINUE
1210 IF (LNC1.EQ.0) GO TO 300
1220 IF (LNC1.GT.0) GO TO 300
1230 IF (LNC1.EQ.1) GO TO 300
1240 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
1250 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
1260 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
1270 CONTINUE
1280 IF (LNC1.EQ.0) GO TO 300
1290 IF (LNC1.GT.0) GO TO 300
1300 IF (LNC1.EQ.1) GO TO 300
1310 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
1320 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
1330 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
1340 CONTINUE
1350 IF (LNC1.EQ.0) GO TO 300
1360 IF (LNC1.GT.0) GO TO 300
1370 IF (LNC1.EQ.1) GO TO 300
1380 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
1390 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
1400 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
1410 CONTINUE
1420 IF (LNC1.EQ.0) GO TO 300
1430 IF (LNC1.GT.0) GO TO 300
1440 IF (LNC1.EQ.1) GO TO 300
1450 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
1460 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
1470 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
1480 CONTINUE
1490 IF (LNC1.EQ.0) GO TO 300
1500 IF (LNC1.GT.0) GO TO 300
1510 IF (LNC1.EQ.1) GO TO 300
1520 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
1530 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
1540 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
1550 CONTINUE
1560 IF (LNC1.EQ.0) GO TO 300
1570 IF (LNC1.GT.0) GO TO 300
1580 IF (LNC1.EQ.1) GO TO 300
1590 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
1600 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
1610 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
1620 CONTINUE
1630 IF (LNC1.EQ.0) GO TO 300
1640 IF (LNC1.GT.0) GO TO 300
1650 IF (LNC1.EQ.1) GO TO 300
1660 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
1670 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
1680 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
1690 CONTINUE
1700 IF (LNC1.EQ.0) GO TO 300
1710 IF (LNC1.GT.0) GO TO 300
1720 IF (LNC1.EQ.1) GO TO 300
1730 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
1740 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
1750 IF (K.GT.KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,280) K,R(I,K)
1760 CONTINUE
1770 IF (LNC1.EQ.0) GO TO 300
1780 IF (LNC1.GT.0) GO TO 300
1790 IF (LNC1.EQ.1) GO TO 300
1800 IF (KPTS(I).AND.K.LE.NLINES) WRITE (LOG2,260) XSTA(K,I),RSTA(
1810 IF (K.LE.KPTS(I).AND.K.GT.NLINES) WRITE (LOG2,270) XSTA(K,I),RSTA(
1820 IF (K.GT.KPTS(I).AND.K
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640 VP(J,I)=PAD(I)*SIN(EPS)
650 XP(J,I)=XTEMP(I)
660 I=1,31
670 XTEMP(I)=XSEMI(J,I)
680 CALL UD0315 (SS,X,100,XTEMP,XTEMP,31,1)
690 CALL UD0315 (XH,Z,100,XTEMP,XTEMP,31,1)
700 X=3
710 DO 690 I=1,31
720 EPS=EPZ(I,K)
730 YSEMI(J,I)=RAD(I)*COS(EPS)
740 YSEMI(J,I)=RAD(I)*SIN(EPS)
750 XSEMI(J,I)=XTEMP(I)
760 IF (ISECH.NL,2) GO TO 690
770 XTEMP(I)=XSEMI(J,I)
780 CALL UD0315 (SS,X,100,XTEMP,XTEMP,31,1)
790 CALL UD0315 (XH,Z,100,XTEMP,XTEMP,31,1)
800 X=4
810 DO 690 I=1,31
820 EPS=EPZ(I,K)
830 YSEMI(J,I)=RAD(I)*COS(EPS)
840 YSEMI(J,I)=RAD(I)*SIN(EPS)
850 XSEMI(J,I)=XTEMP(I)
860 IF (IPRINT,6,2) GO TO 670
870 IF (LNCT,12,5) GO TO 700
880 KRITE (LOG2,200)
890 LNCT=LNCT+1
900 KRITE (LOG2,710)
910 J=J+1
920 IF (LOG2,710) J=J+1
930 IF (LOG2,710) J=J+1
940 IF (LOG2,710) J=J+1
950 IF (LOG2,710) J=J+1
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1080 IF (LOG2,710) J=J+1
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1770 IF (LOG2,710) J=J+1
1780 IF (LOG2,710) J=J+1
1790 IF (LOG2,710) J=J+1
1800 IF (LOG2,710) J=J+1
1810 IF (LOG2,710) J=J+1
1820 IF (LOG2,710) J=J+1
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1840 IF (LOG2,710) J=J+1
1850 IF (LOG2,710) J=J+1
1860 IF (LOG2,710) J=J+1
1870 IF (LOG2,710) J=J+1
1880 IF (LOG2,710) J=J+1
1890 IF (LOG2,710) J=J+1
1900 IF (LOG2,710) J=J+1
1910 IF (LOG2,710) J=J+1
1920 IF (LOG2,710) J=J+1
1930 IF (LOG2,710) J=J+1
1940 IF (LOG2,710) J=J+1
1950 IF (LOG2,710) J=J+1
1960 IF (LOG2,710) J=J+1
1970 IF (LOG2,710) J=J+1
1980 IF (LOG2,710) J=J+1
1990 IF (LOG2,710) J=J+1
2000 IF (LOG2,710) J=J+1

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770 WRITE (LOG2,740)
780 FORMAT (2X,/,10X,5HPPOINT NO,4X,5HZSEMI,9X,5HXSEMI,9X,5HYSEMI,/,2X)
790 EQUIVALENT (2X,/,10X,5HPPOINT NO,4X,5HZSEMI,9X,5HXSEMI,9X,5HYSEMI,/,2X)
147SEMI,9X,5HZSEMI,9X,5HXSEMI,9X,5HYSEMI,/,2X)
800 WRITE (LOG2,740)
810 FORMAT (10X,/,3X,1P3F14.5)
820 WRITE (LOG2,740)
830 WRITE (LOG2,740)
840 WRITE (LOG2,740)
850 WRITE (LOG2,740)
860 WRITE (LOG2,740)
870 WRITE (LOG2,740)
880 WRITE (LOG2,740)
890 WRITE (LOG2,740)
900 WRITE (LOG2,740)
910 WRITE (LOG2,740)
920 WRITE (LOG2,740)
930 WRITE (LOG2,740)
940 WRITE (LOG2,740)
950 WRITE (LOG2,740)
960 WRITE (LOG2,740)
970 WRITE (LOG2,740)
980 WRITE (LOG2,740)
990 WRITE (LOG2,740)

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```

1P(1H*))
IF (IDUM.EQ.0) GO TO 1030
IF (IPRINT.NE.3) WRITE (LOG2,200)
IF (IPRINT.EQ.3) WRITE (LOG2,910)
FORMAT (2X,/,2X)
WRITE (LOG2,920)
FORMAT (43X,/,3HBLADE CALCULATIONS FOR AERODYNAMIC ANALYSIS,/,43X,4
13(1H*))
IDUM=7
LNCT=LNCT+4
IF (IPRINT.NE.3) LNCT=3
GO 1020 IF 1, NSTNS
IF (IFANGS(I).EQ.0 .OR. (ISPLIT.GE.1.AND. IFANGS(I).EQ.1)) GO TO 1020
GO 940 IF 1, NLINES
CALL UD0315 (RSTA(1,I),XSTA(1,I),KPTS(I),K(I,J),XDUM,1,0)
CALL UD0315 (RSTA(1,I),XSTA(1,I),KPTS(I),R(I,J),XDUM,2Q(J),1,1)
DO 930 K=1,NPOINT
  XAD(K)=XS(J,K)
  XTEMP(K)=YS(J,K)
  X(K)=YP(J,K)
  XDUM=XDUM-STACKX
CALL UD0315 (SS,RAD,NPOINT,XDUM,YY1,1,1)
CALL UD0315 (XTEMP,X,NPOINT,XDUM,YY2,1,1)
W1=YY1/R(I,J)
W2=YY2/R(I,J)
TU(J)=A3S(AT1J(W1/SORT(1.-W1**2))-ATAN(W2/SORT(1.-W2**2)))/(2.*PI)
1*FLOAT(NBLADE)
CONTINUE
CALL UD0315 (/CAMB(1,I),YCAMB(1,I),NLINES,ZCAMB(1,I),XDUM,RLE,NLINES,1)
IF (LNCT+IDUM+NLINES.LE.59) GO TO 950
WRITE (LOG2,200)
LNCT=LNCT+IDUM+NLINES
WRITE (LOG2,950) I, NLINES
FORMAT (//,/,4X,3HSTATION,12,5X,17HNUMBER OF RADII=,12,/,36X,6H
RADIIU,5X,7HSECTION,5X,4HLEAN,9X,5HBLADE,7X,5HTHETA,/,48X,5HANGLE,
20X,5HANGLE,7X,8H3LOCKAGE,/,2X)
DO 1000 J=1,NLINES
  EPS=(THETA(J,I)-ATAN(RLE(J)))*C1
  ALPHR=ALPHA(J,I)
  ALP=(ATAN(TANPHI(I,J)*TAN(EPS/C1))+ALPHR*SQRT(1.+TANPHI(I,J)**2))/
  1(1.-TANPHI(I,J)*ZQ(J)))*C1
  ALPRL(J,J)=ALP
  ALPSLON(I,J)=ATAN(TAN(EPS/C1)/SQRT(1.0+ZQ(J)**2))*C1
IF (ISPLIT.LT.1) GO TO 990
FORMAT (LOG2,970) X3
FORWRITE (LOG2,970) X3,I,J

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```

980  FORMAT(90X,14HADJUST. BLOCK =,F7.5,3H I=,I2,3H J=,I2)
990  T(J)=TQ(J)+K
1000  WRITE (LOG2,1J10) R(I,J),ALF,_PS,TQ(J),THETA(J,I)
1010  BLOCK(I,J)=I2(J)
1020  FORMAT(30X,3F12.4)
1030  CONTINUE
1040  IF (IFPLOT.LI.2.OR.IFPLOT.EQ.7) GO TO 1045
1050  CALL UD0317 (ISTAK,PLTISZ,2,TITLE,IKUUM,IFPLOT)
1060  IF (IPRINT.EQ.1.OR.IPRINT.EQ.3) GO TO 1050
1070  LNCY=2
1080  WRITE (LOG2,1050)
1090  FORMAT (1H1,27X,74HBLADE SURFACE GEOMETRY IN CARTESIAN COORDINATES
1100  1 AT SPECIFIC VALUES OF {Z(,/,28X,74H*****))
1110  2 *****
1120  IF (IPRINT.EQ.1.AND.IFPLOT.LE.1) GO TO 1470
1130  XZ=NZ-1
1140  Z=(ZOUT-1)*ZINNER/XZ
1150  ZOUT(1)=ZIN
1160  DO 1070 J=3,NZ
1170  ZOUT(J)=ZOUT(J-1)+DZ
1180  ZOUT(NZ)=ZOUT(NZ-1)*POINT
1190  DO 1040 I=1,NPOINT
1200  CALL UD0315 (ZS(I,I),XSI(1,I),NLINES,ZOUT,TEMP1,NZ,0)
1210  CALL UD0315 (ZS(I,I),YSI(1,I),NLINES,ZOUT,TEMP2,NZ,0)
1220  CALL UD0315 (ZP(I,I),XPI(1,I),NLINES,ZOUT,TEMP3,NZ,0)
1230  CALL UD0315 (ZP(I,I),YPI(1,I),NLINES,ZOUT,TEMP4,NZ,0)
1240  DO 1040 J=1,NZ
1250  XS(J,I)=TEMP1(J)
1260  YS(J,I)=TEMP2(J)
1270  XP(J,I)=TEMP3(J)
1280  YP(J,I)=TEMP4(J)
1290  DO 1090 I=1,31
1300  XSEMI(1,I),XSEMI(1,I),NLINES,ZOUT,TEMP1,NZ,0)
1310  CALL UD0315 (ZSEMI(1,I),YSEMI(1,I),NLINES,ZOUT,TEMP2,NZ,0)
1320  XSEMI(J,I)=TEMP1(J)
1330  YSEMI(J,I)=TEMP2(J)
1340  IF (ISELN.NE.2) GO TO 1110
1350  DO 1100 I=1,31
1360  XSEMI(1,I)=TEMP1(J)
1370  CALL UD0315 (ZSEMI(1,I),YSEMI(1,I),NLINES,ZOUT,TEMP1,NZ,0)
1380  CALL UD0315 (ZSEMI(1,I),YSEMI(1,I),NLINES,ZOUT,TEMP2,NZ,0)
1390  XSEMI(J,I)=TEMP1(J)
1400  YSEMI(J,I)=TEMP2(J)
1410  DO 1420 J=1,NZ
1420  X=XP(J,I)-YP(J,I)**2+(YS(J,I)-YP(J,I)**2)/2.0
1430  Y=YS(J,I)+XP(J,I)-YP(J,I)/(XS(J,I)+XP(J,I)-XS(J,I)+YP(J,I)*RQ)
1440  AREA=PI*RQ**2/2.0
1450  RETAI=ATAN((YS(J,I)-YP(J,I))/(XS(J,I)+XP(J,I)-XS(J,I)+YP(J,I)*RQ))
1460  1,111-XP(J,I)
1470  XINT=ARETA*(((XP(J,I)+XS(J,I))/2.0-COS(BETA1)*4.0/(3.6*PI)*RQ)

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1120 YINT=AP*A*((YP(J,1)+YS(J,1))/2.0-SIN(BETA1))*4.0/(3.0*PI)*RD)
IF (ISECON.NE.2) GO TO 1120
N1=NPOINT
N2=N1-1
R1A2=ATAN((YS(J,N1)+YP(J,N2)-YS(J,N2))/(XS(J,N1)+XP(J,N1)
1) -XS(J,N2)-XP(J,N2)))
XINT=XINT+AP*A*((XP(J,N1)+XS(J,N1))/2.+COS(BETA2)*4.0/(3.0*PI)*RD)
YINT=YINT+AP*A*((YP(J,N1)+YS(J,N1))/2.+SIN(BETA2)*4.0/(3.0*PI)*RD)
AREA=2.*AP*A
GO 1130 I=2, NPOINT
DELTA=(SQRT((XS(J,I)-XS(J,I-1))**2+(YS(J,I)-YP(J,I-1))**2)+SQRT((XS(J,I)-XS(J,I-1))**2+(YS(J,I)-YP(J,I-1))**2))/4.0
AREA=AREA+DELTA
XINT=XINT+DELTA*(XS(J,I)+XS(J,I-1)+XP(J,I)+XP(J,I-1))/4.0
YINT=YINT+DELTA*(YS(J,I)+YS(J,I-1)+YP(J,I)+YP(J,I-1))/4.0
XINT=XINT/AREA
YINT=YINT/AREA
X1=(XS(J,1)+XP(J,1))/2.
Y1=(YS(J,1)+YP(J,1))/2.
I1=SQRT((XS(J,1)-XP(J,1))**2+(YS(J,1)-YP(J,1))**2)
U=0.
GO 1140 I=2, NPOINT
I2=SQRT((XS(J,I)-XP(J,I))**2+(YS(J,I)-YP(J,I))**2)
X2=(XS(J,I)+XP(J,I))/2.
Y2=(YS(J,I)+YP(J,I))/2.
DELTA=SQRT((X2-X1)**2+(Y2-Y1)**2)
U=U+DELTA
TAV3=(I1**3+I2**3)/2.
F=U+TAV3*DELTA
X1=X2
Y1=Y2
I1=I2
TCON=((1./3.)*F)/(1.+(./3.)*F/AREA/U**2)
IX=0.0
IY=0.0
IXY=0.0
GO 1150 I=2, NPOINT
X2=(SQRT((XS(J,I)-XP(J,I))**2+(YS(J,I)-YP(J,I-1))**2)+SQRT((XS(J,I)-XP(J,I))**2+(YS(J,I)-YP(J,I-1))**2))/2.0
Y2=(SQRT((XS(J,I)-XP(J,I))**2+(YS(J,I)-YP(J,I-1))**2)+SQRT((XS(J,I)-XP(J,I))**2+(YS(J,I)-YP(J,I-1))**2))/2.0
IXY=XY+X2*Y2/2.0
IYD=X2*Y2/2.0
ANG=ATAN((YS(J,I)+YP(J,I)-YS(J,I-1)+YP(J,I-1))/(XP(J,I)+XP(J,I-1)-XP(J,I-1)-XP(J,I-1)))
1 COSANG=COS(2.*ANG)

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[illegible]


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45 13H F7.5,6H AXCE=F7.3)
50 WRITE(LOG2,5J)IHL,P,Q,BETA1,BETA2,YZERO,T,YONE,Z,AXIALC
55 13H F7.5,6H AXCE=F7.3)
60 13H F7.5,6H AXCE=F7.3)
70 13H F7.5,6H AXCE=F7.3)
80 13H F7.5,6H AXCE=F7.3)
90 13H F7.5,6H AXCE=F7.3)
100 13H F7.5,6H AXCE=F7.3)

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```

110      G1=GR3      100
      GO TO 100
120      G2=GR3      100
      GO TO 100
      A2=G3
      A1=ATN(SB/C1)-TAN(SB/C1))/(1.0-(A1*SQ+1.0)*EXP(-A1*SQ))
      C1=1/TAN(SB/C1)+11/A1**2
      E1=(A1*SQ+2.0)*B1/A1**3*EXP(-A1*SQ)
      B2=A2**2*(TAN(BETA2/C1)-TAN(SB/C1))/(1.0+(A2*(1.0-SQ)-1.0)*EXP(A2*
1      (1.0-SQ)))
      CC2=TAN(SB/C1)+32/A2**2
      D2=2.0*(C2/A2**3-B1/A1**3)+SQ*(CC1-CC2)+E1
      XD=1.0-SQ
      R2=F3(A2,N2,CC2,D2)
      XMLC=SQRT(1.0+R2**2)
      GO TO 100
130      I1=1
      I2=3-B-TA1+39
      GO TO 100
      XD=0.
      YD=0.
      Y2=FLUOAT(N)*SQ
      IF (I2.LE.1) SQ=0.0
      IF (I2.LE.1) BETA3=BETA1
      IF (I2.LE.1) GO TO 140
      XRNGE=SQ
      FACT=SQ
      CALL UD0313 (BETA1,BETA3,I1,I2,FACT,XD,YD,SQ,XRNGE,Y11,X11,Y21,RDI
1      US1,S,C1)
      I1=I2
      YD=Y21
      SQ=SQ(I1)
      I2=N
      FACT=1.-SQ
      XRNGE=FACT
      CALL UD0313 (BETA3,BETA2,I1,I2,FACT,XD,YD,SQ,XRNGE,Y12,X12,Y22,RDI
1      US2,S,C1)
      XMLC=SQRT(1.0+Y22**2)
      GO TO 100
140      CALL UD0313 (BETA1,BETA2,1,N,1.0,0.0,0.0,0.0,1.0,Y1,X1,Y2,RDIUS,S,
      C1)
      XMLC=SQRT(1.0+Y2**2)
      CHORD=XMLC/(1.-2.*YZERO*(1.-XMLC))
      FOCUS=1.0-CHORD**2.+YZERO
      GO TO 170

```

```

160 CHORD=X*YLC/(1.0-YZERO+XMLC*(YZERO+ABS(YONE* SIN(BETA2/C1))))
170 FCSLXN=1.0-CHORD*(YZERO+ABS(YONE* SIN(BETA2/C1)))
    YZERO=YZERO+CHORD/FCSLMN
    YONE=YONE+CHORD/FCSLMN
    I=1+CHORD/FCSLMN
    I(1)=0.0
    XX=0.0
    XN=1.0
    IF (ISECN-50.2) GO TO 240
    IT=(YZERO-T/2.0)/(2.0*Z**3)
    CT=(T/2.0-YZERO)*3.0/(2.0*Z)
    QT=(YZERO-T/2.0)/(Z**2)
    ET=1.0*(YZERO-T/2.0)/Z**2
    HT=(ISECN-50.3) GO TO 240
    DELX=1.0/(10.0*(XN-1.0))
    ASSIGN 190 TO ISEC1
    ASSIGN 290 TO ISEC2
    ASSIGN 300 TO ISEC1
    ASSIGN 300 TO ISEC2
    DO 230 JJ=1,11
    GO TO ISEC1 (190,200)
    PHI(JJ)=SQRT(1.0+(CA/12.0*(XX-H)**3+XK2*2.0*XX+8)**2)
    X0=XX-SQ
    IF (X0.GT.0.1) GO TO 210
    PHI(JJ)=SQRT(1.0+(F5(A1,B1,CC1))**2)
    GO TO 220
    PHI(JJ)=SQRT(1.0+(F5(A2,B2,CC2))**2)
    XX=XX+DELX
    S(JJ)=S(J-1)+(PHI(1)+PHI(11))+4.0*(PHI(2)+PHI(4)+PHI(6)+PHI(8)+PHI(10)
131)+2.0*(PHI(3)+PHI(5)+PHI(7)+PHI(9)))/(30.0*(XN-1.0))
    DELX=1.0/(XN-1.0)
    IF (ISECN-50.2) GO TO 250
    IT2=T/2.0-YZERO
    TPRIM2=C1
    AFORM=1.0-COS((BETA1-BETA2)/C2))/(1.0+AFORM**2)
    PHIS=ACOS(1.0-AFORM**2)/(1.0+AFORM**2)
    RYSS=RO+XMLC/2.0/SIN(PHIS)
    YSS=RO+XMLC/2.0/SIN(PHIS)
    AFORM=1.0-COS((BETA1-BETA2)/C2))-TPRIM2/XMLC*2.0
    PHIP=ACOS(1.0-AFORM**2)/(1.0+AFORM**2)
    PHIP2=ABS((BETA1-BETA2)/C1)
    PHI(1)=0.0

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360      IF (BTAT1-BTAT2).LT.0.0) YPRIME=-YPRIME
      IF (ISCON.EQ.3) GO TO 370
      IF (J.EQ.13) DELX=DELXX
      YPRIME=ATAN(BETA3/C1)
      IF (J.NE.1) X4M=X4(J-1)/FCSLMN-YZERO
      IF (J.NE.1) Y4M=Y4(J-1)/FCSLMN
      Y4(J)=YPRIME*(X4(J)-X4M)+Y4M
      IF (J.EQ.13) DELX=DELXX
      X4(J+1)=X4(J)+DELX
      Y4(J+1)=Y4(J)+DELX
      FYP=1.0/SQRT(1.0+YPRIME**2)
      X5(I8L,J)=(X4(J)-THICK2(J))*YPRIME*FYP+YZERO)*FCSLMN
      X5(I8L,J)=(Y4(J)+THICK2(J))*FYP*FCSLMN
      X6(I8L,J)=(X4(J)+THICK2(J))*YPRIME*FYP+YZERO)*FCSLMN
      X6(I8L,J)=(Y4(J)-THICK2(J))*FYP*FCSLMN
      X4M(J)=ATAN(YPRIME)*C1
      X4(J)=X4M(J)
      IF (J.EQ.N) STAGER=ATAN(Y4(N)/X4(N))*C1
      X4M(J)=(X4(J)+YZERO)*FCSLMN
      X5M(J)=Y4(J)*FCSLMN
      THICK2(J)=THICK2(J)*FCSLMN
      S(J)=S(J)*FCSLMN
      IF (ISPLIT.EQ.0) GO TO 530
      XSPLTM(1)=1.-PERSPJ
      XSPLTM(K1)=1.
      X11=X1-1
      DELXX=1-PERSPJ/FLOAT(K11)
      DO 390 J=2,K11
      XSPLTM(J)=XSPLTM(J-1)+DELXX
      CALL UD0315 (XM,Y4,N,XSPLTM,YSPSTM,K1,1)
      CALL UD0315 (XM,Y4,N,XSPLTM,K1,1)
      CALL UD0315 (XM,AM,N,XSPLTM,SS1(1,3),K1,1)
      XSPLMS=XSPLTM(1)
      DO 400 J=1,K1
      XSPLTM(J)=XSPLMS
      XSPLTM(410,420)=XSPLTM(K11)-XSPLTM(11)*2+(YSPLTM(K11)-YSPLTM(11))*2)
      XNORMS=SQRT(1+(XSPLTM(11)-XNORMS+XNORMS*(YZEROS+ABS(YONES*SIN(BETA2/C1))))/PERSPJ)
      CHOROS=XNORMS/(1.-YZEROS*(YZEROS+ABS(YONES*SIN(BETA2/C1))))/PERSPJ
      YZEROS=(YZEROS+CHOROS)/FCSLMS
      YONES=YONES+CHOROS/FCSLMS
      TS=(Y4/2.-YZEROS)/(1.-YZEROS)
      AT=(TS/2.-YZEROS)
      CT=(Y4/2.-YZEROS)
      ZSPMX1=ZSPMX1*(1.-ZSPMX1)*3-1.5*(YZEROS-TS/2.)/(ZSPMX1**2*(1.-ZSPMX1))

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[illegible]

[illegible]

[illegible]

170	YPRIME(I)=(-M(J)*(XDATA(J+1)-XIN(I))*2/2.0+M(J+1)*(XIN(I)-XDATA(J	52
180	1))**2/2.0+YDATA(J+1)-YDATA(J))/DX-(M(J+1)-M(J))/6.0*DX	53
190	IF (I-NXY) 1JU,100,240	54
	YDASH=(YDATA(2)-YDATA(1))/(XDATA(2)-XDATA(1))-(M(1)/3.0+M(2)/6.0)*	55
200	1(XDATA(2)-XDATA(1))	56
	IF (NWOI-1) 200,210,200	57
210	YOUT(I)=YDATA(1)-YDASH*(XDATA(1)-XIN(I))	58
	IF (NWOI) 210,190,210	59
220	YPRIME(I)=YOUT(I)	60
	GO TO 180	61
	YDASH=(YDATA(NDATA)-YDATA(N))/(XDATA(NDATA)-XDATA(N))+ (M(NDATA)/3.0	62
230	1+M(N)/6.0)*(XDATA(NDATA)-XDATA(N))	63
	IF (NWOI-1) 230,210,230	64
240	YOUT(I)=YDATA(NDATA)+YDASH*(XIN(I)-XDATA(NDATA))	65
	IF (NWOI) 210,190,210	66
	RETURN	67
	END	68

220	IF (XIN(I)-XDATA(NDATA)) 280,270,240	23
230	JP=1	5
	KP=2	5
240	GO TO 250	5
	JP=NDATA	5
250	KP=NDATA-1	5
	VPRIME=(YDATA(KP)-YDATA(JP))/(XDATA(KP)-XDATA(JP))-M(KP)/6.0*(XDATA	5
	1A(KP)-XDATA(JP))	5
	YOUT(I)=YDATA(JP)+(XIN(I)-XDATA(JP))*VPRIME	5
260	GO TO 350	5
	YOUT(I)=YDATA(I)	5
270	GO TO 350	5
	YOUT(I)=YDATA(NDATA)	5
280	GO TO 350	5
290	IF (XIN(I)-XDATA(J)) 300,320,290	5
300	IF (XIN(I)-XDATA(J+1)) 340,330,300	5
	J=J+1	5
310	IF (J-NDATA) 260,310,310	5
	J=1	5
320	GO TO 280	5
	YOUT(I)=YDATA(J)	5
330	GO TO 350	5
	YOUT(I)=YDATA(J+1)	5
340	GO TO 350	5
	DX=XDATA(J+1)-XDATA(J)	5
	YOUT(I)=M(J)/(6.0*DX)*(XDATA(J+1)-XIN(I))+3*M(J+1)/(9.0*DX)*(XIN	5
	1I)-XDATA(J))+3*(XDATA(J+1)-XIN(I))*(YDATA(J)/DX-M(J)/6.0*DX)+(XIN	5
	2(I)-XDATA(J))*(YDATA(J+1)/DX-M(J+1)/6.0*DX)	5
350	IF (I-NXY) 350,370,370	5
360	I=I+1	5
	GO TO 210	5
370	RETURN	5
	END	5


```

30      LINE(L)=3*LAN<
      IF (KLINE.EQ.7.OR.KLINE.EQ.13.OR.KLINE.EQ.19.OR.KLINE.EQ.25.OR.KLI
1     VE.EQ.31.OR.KLINE.EQ.37.OR.KLINE.EQ.43.OR.KLINE.EQ.49) GO TO 40
      LINE(1)=XI
      LINE(121)=XI
      GO TO 40
      LINE(1)=DASH
      LINE(121)=DASH
      GO TO 30
      L=2,120
      LINE(L)=DASH
      LINE(1)=CROSS
      LINE(121)=CROSS
      GO TO 70
      L=11,111,10
      LINE(L)=XI
      GO TO 120
      GO TO 100
      I=1,X,YH+YINC2,OR,Y2(I),LE,YH-YINC2) GO TO 90
      IF (Y2(I)-XL)/X RANGE+120.0+1.5
      LINE(L)=SYMBOL
      IF (Y1(I)-XL)/YH+YINC2,OR,Y1(I),LE,YH-YINC2) GO TO 100
      L=(X1(I)-XL)/X RANGE+120.0+1.5
      LINE(L)=SYMBOL
      CONTINUE
      IF (KLINE.EQ.1.OR.KLINE.EQ.7.OR.KLINE.EQ.13.OR.KLINE.EQ.19.OR.KLI
1     VE.EQ.25.OR.KLINE.EQ.31.OR.KLINE.EQ.37.OR.KLINE.EQ.43.OR.KLINE.EQ.4
2     9.OR.KLINE.EQ.55) GO TO 120
      WRITE (LOG1,110) LINE
      FORMAT (9X,121A1)
      GO TO 120
      YNUM=YH*10.0**MY
      WRITE (LOG1,130) YNUM,LINE
      FORMAT (1X,F3.3,1X,121A1)
      YH=YH-YINC
      XNUM(1)=XL*10.0**MX
      XINC=((XH-XL)/12.0)*10.0**MX
      GO TO 150
      XNUM(I)=XNUM(I-1)+XINC
      XNUM(150)=XNUM(150)
      WRITE (LOG1,150) XNUM
      FORMAT (6X,12(F5.3,'X'),F0.3)
      RETURN
      IF (LOG1,140)
      WRITE (//,3X,54H+0 PLOT HAS BEEN MADE BECAUSE (XC OR (YC RANGE
1     IS ZERO)
      END

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\$17\$ 52

END


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SUBROUTINE UJ0313 (LOG1,LOG2,LOG3,LOG5,NLINES,NSPEC,KPTS,RSIA,XSTIA,
1XR,78,81,82,FC,PI,31,NBLADE,CORD,BLOCK,ALP9,EPSON,IFANGS,IPUNCH,
2DIMENS)
1) R(1), R2(1), R3(1), R4(1), R5(1), R6(1), R7(1), R8(1), R9(1), R10(1), R11(1), R12(1), R13(1), R14(1), R15(1), R16(1), R17(1), R18(1), R19(1), R20(1), R21(1), R22(1), R23(1), R24(1), R25(1), R26(1), R27(1), R28(1), R29(1), R30(1), R31(1), R32(1), R33(1), R34(1), R35(1), R36(1), R37(1), R38(1), R39(1), R40(1), R41(1), R42(1), R43(1), R44(1), R45(1), R46(1), R47(1), R48(1), R49(1), R50(1), R51(1), R52(1), R53(1), R54(1), R55(1), R56(1), R57(1), R58(1), R59(1), R60(1), R61(1), R62(1), R63(1), R64(1), R65(1), R66(1), R67(1), R68(1), R69(1), R70(1), R71(1), R72(1), R73(1), R74(1), R75(1), R76(1), R77(1), R78(1), R79(1), R80(1), R81(1), R82(1), R83(1), R84(1), R85(1), R86(1), R87(1), R88(1), R89(1), R90(1), R91(1), R92(1), R93(1), R94(1), R95(1), R96(1), R97(1), R98(1), R99(1), R100(1), R101(1), R102(1), R103(1), R104(1), R105(1), R106(1), R107(1), R108(1), R109(1), R110(1), R111(1), R112(1), R113(1), R114(1), R115(1), R116(1), R117(1), R118(1), R119(1), R120(1), R121(1), R122(1), R123(1), R124(1), R125(1), R126(1), R127(1), R128(1), R129(1), R130(1), R131(1), R132(1), R133(1), R134(1), R135(1), R136(1), R137(1), R138(1), R139(1), R140(1), R141(1), R142(1), R143(1), R144(1), R145(1), R146(1), R147(1), R148(1), R149(1), R150(1), R151(1), R152(1), R153(1), R154(1), R155(1), R156(1), R157(1), R158(1), R159(1), R160(1), R161(1), R162(1), R163(1), R164(1), R165(1), R166(1), R167(1), R168(1), R169(1), R170(1), R171(1), R172(1), R173(1), R174(1), R175(1), R176(1), R177(1), R178(1), R179(1), R180(1), R181(1), R182(1), R183(1), R184(1), R185(1), R186(1), R187(1), R188(1), R189(1), R190(1), R191(1), R192(1), R193(1), R194(1), R195(1), R196(1), R197(1), R198(1), R199(1), R200(1), R201(1), R202(1), R203(1), R204(1), R205(1), R206(1), R207(1), R208(1), R209(1), R210(1), R211(1), R212(1), R213(1), R214(1), R215(1), R216(1), R217(1), R218(1), R219(1), R220(1), R221(1), R222(1), R223(1), R224(1), R225(1), R226(1), R227(1), R228(1), R229(1), R230(1), R231(1), R232(1), R233(1), R234(1), R235(1), R236(1), R237(1), R238(1), R239(1), R240(1), R241(1), R242(1), R243(1), R244(1), R245(1), R246(1), R247(1), R248(1), R249(1), R250(1), R251(1), R252(1), R253(1), R254(1), R255(1), R256(1), R257(1), R258(1), R259(1), R260(1), R261(1), R262(1), R263(1), R264(1), R265(1), R266(1), R267(1), R268(1), R269(1), R270(1), R271(1), R272(1), R273(1), R274(1), R275(1), R276(1), R277(1), R278(1), R279(1), R280(1), R281(1), R282(1), R283(1), R284(1), R285(1), R286(1), R287(1), R288(1), R289(1), R290(1), R291(1), R292(1), R293(1), R294(1), R295(1), R296(1), R297(1), R298(1), R299(1), R300(1), R301(1), R302(1), R303(1), R304(1), R305(1), R306(1), R307(1), R308(1), R309(1), R310(1), R311(1), R312(1), R313(1), R314(1), R315(1), R316(1), R317(1), R318(1), R319(1), R320(1), R321(1), R322(1), R323(1), R324(1), R325(1), R326(1), R327(1), R328(1), R329(1), R330(1), R331(1), R332(1), R333(1), R334(1), R335(1), R336(1), R337(1), R338(1), R339(1), R340(1), R341(1), R342(1), R343(1), R344(1), R345(1), R346(1), R347(1), R348(1), R349(1), R350(1), R351(1), R352(1), R353(1), R354(1), R355(1), R356(1), R357(1), R358(1), R359(1), R360(1), R361(1), R362(1), R363(1), R364(1), R365(1), R366(1), R367(1), R368(1), R369(1), R370(1), R371(1), R372(1), R373(1), R374(1), R375(1), R376(1), R377(1), R378(1), R379(1), R380(1), R381(1), R382(1), R383(1), R384(1), R385(1), R386(1), R387(1), R388(1), R389(1), R390(1), R391(1), R392(1), R393(1), R394(1), R395(1), R396(1), R397(1), R398(1), R399(1), R400(1), R401(1), R402(1), R403(1), R404(1), R405(1), R406(1), R407(1), R408(1), R409(1), R410(1), R411(1), R412(1), R413(1), R414(1), R415(1), R416(1), R417(1), R418(1), R419(1), R420(1), R421(1), R422(1), R423(1), R424(1), R425(1), R426(1), R427(1), R428(1), R429(1), R430(1), R431(1), R432(1), R433(1), R434(1), R435(1), R436(1), R437(1), R438(1), R439(1), R440(1), R441(1), R442(1), R443(1), R444(1), R445(1), R446(1), R447(1), R448(1), R449(1), R450(1), R451(1), R452(1), R453(1), R454(1), R455(1), R456(1), R457(1), R458(1), R459(1), R460(1), R461(1), R462(1), R463(1), R464(1), R465(1), R466(1), R467(1), R468(1), R469(1), R470(1), R471(1), R472(1), R473(1), R474(1), R475(1), R476(1), R477(1), R478(1), R479(1), R480(1), R481(1), R482(1), R483(1), R484(1), R485(1), R486(1), R487(1), R488(1), R489(1), R490(1), R491(1), R492(1), R493(1), R494(1), R495(1), R496(1), R497(1), R498(1), R499(1), R500(1), R501(1), R502(1), R503(1), R504(1), R505(1), R506(1), R507(1), R508(1), R509(1), R510(1), R511(1), R512(1), R513(1), R514(1), R515(1), R516(1), R517(1), R518(1), R519(1), R520(1), R521(1), R522(1), R523(1), R524(1), R525(1), R526(1), R527(1), R528(1), R529(1), R530(1), R531(1), R532(1), R533(1), R534(1), R535(1), R536(1), R537(1), R538(1), R539(1), R540(1), R541(1), R542(1), R543(1), R544(1), R545(1), R546(1), R547(1), R548(1), R549(1), R550(1), R551(1), R552(1), R553(1), R554(1), R555(1), R556(1), R557(1), R558(1), R559(1), R560(1), R561(1), R562(1), R563(1), R564(1), R565(1), R566(1), R567(1), R568(1), R569(1), R570(1), R571(1), R572(1), R573(1), R574(1), R575(1), R576(1), R577(1), R578(1), R579(1), R580(1), R581(1), R582(1), R583(1), R584(1), R585(1), R586(1), R587(1), R588(1), R
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360      NX=LOG2(0.3),J,NX=L'CG3
      IF(MAT(NX,330))LITEP(I),NMACH(I),MLOSS(I),NL1(I),NL2(I),NEVAL
      1(I),CURVE(I),NLITEP(I),NOUT1(I),NOUT2(I),NOUT3(I),NBLAD(I)
      2(I),SPEC'D,(P(I,J)),DELTAU(J),EPSLN(I,J),BLOCK(I,J),SOL(J),
      3DEF(NX,J),J=1,NLITE3
      IF(NX)=J.LOG3)GO TO 370
      NX=LOG3
      IF(MAERJ.NE.0.AND.IPUNCH.NE.0)GO TO 360
      COMTIME
      FORMAT(2I3,34 0,I3,3H 6,1I3,/ ,F12.3,/ ,F12.7,/ ,F12.7,36X)
      PRINTN
      END

```



```

150 X, IH=, I3, /, 10X, 3H I V A S T, 25X, 1H=, I3)
160 READ (LOG1, 130) Z I N N E R, Z O U T E R, S C A L E, S T A C K X, P L T S Z E
WRITE (LOG2, 130) Z I N N E R, Z O U T E R, S C A L E, S T A C K X, P L T S Z E
FORMAT (5F12.2)
165 10X, 5H S C A L E, 1H=, F8.4, /, 10X, 6H Z O U T E R, 24X, 1H=, F8.4, /,
20X, 5H S C A L E, 1H=, F8.4, /, 10X, 6H P L T S Z, 24X, 1H=, F8.4, /, 10X, 6H P L T S Z
170 READ (LOG1, 130) I R L E, I X T E, N P A D E V, N I N C, N S I G N, I F C A
WRITE (LOG2, 130) I R L E, I X T E, N P A D E V, N I N C, N S I G N, I F C A
FORMAT (10X, 3H I N C, 1H=, I3, /, 10X, 26H R A D I I, 5X, 20H N O R M A L I Z E D
175 10X, 3H I N C, 1H=, I3, /, 10X, 26H R A D I I, 5X, 20H N O R M A L I Z E D
20X, 3H I N C, 1H=, I3, /, 10X, 26H R A D I I, 5X, 20H N O R M A L I Z E D
210 10X, 3H I N C, 1H=, I3, /, 10X, 26H R A D I I, 5X, 20H N O R M A L I Z E D
220 10X, 3H I N C, 1H=, I3, /, 10X, 26H R A D I I, 5X, 20H N O R M A L I Z E D
230 10X, 3H I N C, 1H=, I3, /, 10X, 26H R A D I I, 5X, 20H N O R M A L I Z E D
240 10X, 3H I N C, 1H=, I3, /, 10X, 26H R A D I I, 5X, 20H N O R M A L I Z E D
250 10X, 3H I N C, 1H=, I3, /, 10X, 26H R A D I I, 5X, 20H N O R M A L I Z E D

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260      YSTA(I)=YSTA(1,I)+1.0
      IF (INAST.EQ.0) READ (LOGN,200) (R(I,J),AIRANG(I,J),J=1,NLINES)
      IF (INAST.NE.0) READ (LOGN,270) (P(I,J),AIRANG(I,J),J=
11,NLINES)
270      IDUM=KPTS(I)
      IF (NLINES.GT.IDUM) IDUM=NLINES
      IF (LNCT.LE.34-NLINES) GO TO 290
      WRITE (LOG2,280)
      FORMAT (1H1)
280      LNCT=1
      LNCT=LNCT+IDU4+5
      IF (INAST.NE.0) GO TO 320
      WRITE (LOG2,300) I,KPTS(I),I,IFANGS(I)
      FORMAT (2X,I/,10X,17HCOMPUTING STATION,I3,5X,28HNUMBER OF DESCRIPTION,9X,10HSTR
16 POINTS,I3,2X,7HIFANGS(I,I2,2H)=,I3,/,6X,11HJESCRPTION,9X,10HSTR
29HLINE,I3,5HRAJII,11X,9HAI2 ANGLE,/,6X,1H2,11X,6HNUMBER,/,
3,2X)
      DO 310 K=1,IDUM
      IF (K.LE.KPTS(I),AND,K.LE.NLINES) WRITE (LOG2,320) XSTA(K,I),RSTA(
1K,I),K,P(I,K),AIRANG(I,K)
      IF (K.LE.KPTS(I),AND,K.GT.NLINES) WRITE (LOG2,330) XSTA(K,I),RSTA(
1K,I)
      IF (K.GT.KPTS(I),AND,K.LE.NLINES) WRITE (LOG2,340) K,R(I,K),AIPANG
1(I,K)
      CONTINUE
      FORMAT (3X,F1.4,2X,F1.4,8X,I2,9X,F8.4,9X,F8.4)
310      FORMAT (3X,F1.4,2X,F1.4,2X,F1.4)
320      FORMAT (2X,I2,3X,F1.4,9X,F9.4,3X,F8.4)
      GO TO 330
      WRITE (LOG2,300) I,KPTS(I),I,IFANGS(I)
      FORMAT (2X,I/,10X,17HCOMPUTING STATION,I3,5X,28HNUMBER OF DESCRIPTION,9X,10HSTR
16 POINTS,I3,2X,7HIFANGS(I,I2,2H)=,I3,/,6X,11HJESCRPTION,9X,10HSTR
33HLINE,I3,5HRAJII,11X,9HAI2 ANGLE,5X,14HDELTA PRESSURE,/,6X,1H2,9
34H)
      DO 370 K=1,IDUM
      IF (K.LE.KPTS(I),AND,K.LE.NLINES) WRITE (LOG2,320) XSTA(K,I),RSTA(
1K,I),K,P(I,K),AIRANG(I,K)
      IF (K.LE.KPTS(I),AND,K.GT.NLINES) WRITE (LOG2,330) XSTA(K,I),RSTA(
1K,I)
      IF (K.GT.KPTS(I),AND,K.LE.NLINES) WRITE (LOG2,340) K,R(I,K),AIRANG
1(I,K),AIRANG(I,K)
      CONTINUE
      FORMAT (3X,I2,3X,F1.4,9X,F9.4,3X,F8.4)
370      CONTINUE
      IF (LNCT.LE.34-NLINES) GO TO 330
      WRITE (LOG2,280)
      LNCT=1
      LNCT=LNCT+NS2+5
      READ (LOG1,410) (ZR(J),YA(J),RLE(J),TC(J),TE(J),ZZ(J),DELX(J),DELY
1(J),J=1,NSPE)

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400  FORMAT (6F12.0,/,2F12.0)
410  WRITE (LOG2,10) (ZR(J),YA(J),RLE(J),TC(J),TE(J),ZZ(J),DELX(J),DEL
      1  Y(J),J=1,NSPEC)
      1  MLINE X STACK /,3X,31HSECTION GEOMETRY SPECIFICATIONS,/,9X,95HSTEA
      2  X,6H/CHORD,3X,20H/2*CHORD,3X,8H/2*CHORD,2X,9HMAX THICK,2X,6H/CH
      3  F1,2,F15,/,F11,3,3F12.5,F12.5,F12.5,F12.5)
      4  IF (ISPLIT.EQ.0) GO TO 450
      5  READ (LOG1,420) (RLES(J),TCS(J),TES(J),ZZS(J),PERSPT(J),J=1,NSPEC)
      6  WRITE (LOG2,430)
      7  FORMAT (5F12.0)
      8  DIUS MAX THICK POINT OF PER CENT,/,10X,10HSTREAMLINE,2X,47HLE RA
      9  20R,4X,2H/CHORD,3X,8H/2*CHORD,2X,9HMAX THICK,2X,6H/CHORD,2X,6H/CH
      10 WRITE (LOG2,440) (ZR(J),RLES(J),TCS(J),TES(J),ZZS(J),PERSPT(J),J=1
      11 NSPEC)
      12 FORMAT (10X,F7.2,3X,F9.3,F10.3,3F10.4)
      13 CONTINUE
      14 IF (IFPLOT.EQ.4) CALL PLOT (U,C,-PLTSE,-3)
      15 IF (IFPLOT.EQ.0,OR,IFPLOT.EQ.4) GO TO 460
      16 IKDUM=0
      17 IF (AIRANG(IRLE,1)-AIRANG(IRTE,1)).LT.0.) IKDUM=1
      18 IF (IFPLOT.EQ.1,OR,IFPLOT.EQ.3) CALL UD0324 (ISTAK,PLTSE,1,TITLE,
      19 UD0970 J=1,NLINES
      20 DO 470 I=1,NLINES
      21 XPT=KPTS(I)
      22 CALL UD0322 (XSTA(1,I),XSTA(1,I),KPT,R(I,J),XHERE(I),1,0)
      23 X(1)=XHERE(IRLE)
      24 X(100)=XHERE(IRTE)
      25 AX=(X(200)-X(1))/93.0
      26 DO 480 I=2,93
      27 X(I)=X(1-1)+AX
      28 ICORIT=IRTE-IRLE+1
      29 CALL UD0321 (XHERE(IRLE),K(IRLE,J),ICORIT,X,XOUM,YPRIME,100,1)
      30 S(I)=0
      31 DO 490 I=2,100
      32 S(I)=S(I-1)+AX*SQRT(1.0+((YPRIME(I)+YPRIME(I-1))/2.0)**2)
      33 XJ=J
      34 CALL UD0322 (ZR,TC,NSPEC,XJ,YZ=RO,1,0)
      35 CALL UD0322 (ZR,TE,NSPEC,XJ,YONE,1,0)
      36 CALL UD0322 (ZR,DELY,NSPEC,XJ,XDEL,1,0)
      37 CALL UD0322 (ZR,DELY,NSPEC,XJ,YDEL,1,0)
      38 CALL UD0322 (ZR,ZZ,NSPEC,XJ,Z,SOLID,1,0)
      39 CALL UD0322 (ZR,YA,NSPEC,XJ,SOR,1,0)
      40 CALL UD0322 (ZR,SJIVR,NSPEC,XJ,SOR,1,0)
      41 CALL UD0322 (ZR,YB,NSPEC,XJ,ROLEMN,1,0)

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570 CALL UDU0322 (SM(1,<),DEVCRV(1,K),NPIS(K),S1(L),DEV RAD(K),1,0)
580 CALL UDU0322 (RADCV,DEV RAD,NPAU=V,B(IRIE,J),DEV PCT,1,0)
590 BETHE T(L)=IIRANG(I,J)-DEV*DEV PCT*XSIGN
600 CONTINUE
    I(MN)=I
    ISE=GT-1)*(MN-1)+1
    IPOINT=(INT:GT,F3) IPOINT=40
    IF (IPOINT=GT) IPOINT=1
    X1=1.0/FLCAT(IPOINT-1)
    X0=590 X=1+I(IPOINT)
    SU(K)=FLOAT(X)*X1
    YPME(K)=FLOAT(X)*X1
    YPME(K)=FLOAT(X)*X1
    YPME(K)=FLOAT(X)*X1
    CALL UDU0327 (S1,YPME,MN,SU,X1,X1,IPOINT,0,0)
    CHORD1=SQRT(YU(IPOINT)**2+1.)*SS(100)
    CALL UDU0322 (SU,YU,IPOINT,SSOLID,YSSOLID,1,1)
    CHORD2=SQRT((YU(IPOINT)-SSOLID)**2+(YU(IPOINT)-YSSOLID)**2)*SS(100)
    CHORD1=CHORD1/PI*SS(100)
    CHORD2=CHORD2/PI*SS(100)
    IF (ABS(CHORD1-CHORD2).LT.SOLTOL*SOLID) GO TO 610
    GO TO 530
    IF (IPRINT.NE.2) WRITE (LOG2,540) NN,DEV,SOLID
    IF (IPRINT.NE.2) GO TO 680
    CALL UDU0327 (S1,YPME,MN,SU,X1,YPRI,X1,IPOINT,0,1)
    WRITE (LOG2,550)
    FORMAT (2X,/,5X,21HPOINT NO. FRACTION M,9X,1HY,11X,10HY-D (DEG)
    1,10,630 X=1.0,11HRAU OF CURV,/,2X)
    X1=ATAN(YMPRME(K))*C1
    X2=0.0
    IF (YPRI.ME(K).NE.0.0) X2=(1.0+YMPRI(ME(K)**2)*1.5/YPRI(ME(K)
    WRITE (LOG2,560) K,SU(K),YU(K),X1,YPRI(ME(K),X2
    FORMAT (110,/,F15.6,2X,F14.4)
    WRITE (LOG2,570)
    FORMAT (2X,/,15X,11HDATA POINTS,/,2X)
    DO 660 K=1,MN
    X1=ATAN(YPME(K))*C1
    WRITE (LOG2,570) K,S1(K),X1
    FORMAT (110,/,F16.0,F32.F)
    CONTINUE
    IPOINT=IPOINT/SS(100)
    XVORPC=CHORD1/SS(100)
    AXIALC=SS(100)
    CPT=690 I=1,NPTS
    KPT=KPTS(I)
    CALL UDU0322 (RSTA(1,I),XSTA(1,I),KPT,R(I,J),XHERE(I),1,0)
    X(1)=XHERE(1)
    X(100)=XHERE(NPTS)
    AX=(X(100)-X(1))/99.0

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```

800      DO 810 I=1,NPOINT
810      XTEMP(I)=XS(J,I)
      CALL UD0322 (XS,X,100,XTEMP,XTEMP,NPOINT,1)
      CALL UD0322 (XHERE,R(1,J),NSTVS,XTEMP,RAJ,NPOINT,0)
      XE=1
      DO 820 I=1,NPOINT
820      EPS=EPZ(I,X)
      ZS(J,I)=RAD(I)*COS(EPS)
      XS(J,I)=XTEMP(I)
830      DO 830 I=1,NPOINT
      XTEMP(I)=XP(J,I)
      CALL UD0322 (XS,X,100,XTEMP,XTEMP,NPOINT,1)
      CALL UD0322 (XHERE,R(1,J),NSTVS,XTEMP,RAJ,NPOINT,0)
      XE=2
      DO 840 I=1,NPOINT
840      EPS=EPZ(I,K)
      ZP(J,I)=RAD(I)*COS(EPS)
      YP(J,I)=RAD(I)*SIN(EPS)
      XP(J,I)=XTEMP(I)
850      DO 850 I=1,NPOINT
      XTEMP(I)=XSE4(I,J,I)
      CALL UD0322 (XS,X,100,XTEMP,XTEMP,31,1)
      CALL UD0322 (XHERE,R(1,J),NSTVS,XTEMP,RAJ,31,0)
      XE=3
      DO 860 I=1,31
860      EPS=EPZ(I,K)
      ZSEMI(J,I)=RAD(I)*COS(EPS)
      YSEMI(J,I)=RAD(I)*SIN(EPS)
      XSE(I,PRINT,GE,2) GO TO 970
      IF (LNGT,LE,30) GO TO 970
      WRITE (LOG2,240)
      LNCT=1
870      LNCT=LNGT+5
      WRITE (LOG2,340) J,HCAPIESIAN COORDINATES ON STREAMSURFACE,I3,/,1
880      FORMAT (2X,/,10X,3HCAPIESIAN COORDINATES ON STREAMSURFACE,I3,/,1
      10X,4HPPOINT NJ,5X,2HZ1,12X,2HX1,16X,2HY1,12X,2HZ2,12X,2HY2
      2,/,2X)
      I=1
890      WRITE (LOG2,300) I,ZS(J,I),XS(J,I),YS(J,I),XP(J,I),YP(J,I)
900      FORMAT (10X,I,3X,I3=14.5,4X,I3=14.5)
      I=I+1
      LNCT=LNGT+1
      IF (I,GT,NPOINT) GO TO 920
      IF (LNCT,LE,39) GO TO 990
      WRITE (LOG2,310)
      FORMAT (11H1,9X,8HPPOINT NJ,5X,2HZ1,12X,2HX1,16X,2HZ2,12X,2HY1,12X,2HY2,/,2X)
      1X2,12X,2
      LNCT=2

```



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1120 FORMAT (1H1,27X,74YBLADE SURFACE GEOMETRY IN CARTESIAN COORINATES**
1* AT SPECIFIED VALUES OF (ZC,1,2HX,74H*****),
1130 IF (IPRINT.EQ.1.AND.IFLOT.LE.1) GO TO 1450
XZ=NZ-1
DZ=(ZOUTER-ZINNER)/XZ
DO 1140 J=3,NZ
ZOUT(1)=ZINNER
ZOUT(J)=ZOUT(J-2)+DZ
DO 1150 I=1,NPOINT
CALL UD0322 (ZS(1,I),NLINES,ZOUT,TEMP1,NZ,0)
CALL UD0322 (ZS(1,I),NLINES,ZOUT,TEMP2,NZ,0)
CALL UD0322 (ZP(1,I),NLINES,ZOUT,TEMP3,NZ,0)
CALL UD0322 (ZP(1,I),NLINES,ZOUT,TEMP4,NZ,0)
DO 1150 J=1,NZ
XS(J,I)=TEMP1(J)
YS(J,I)=TEMP2(J)
XP(J,I)=TEMP3(J)
YP(J,I)=TEMP4(J)
DO 1160 I=1,31
XSEMI(1,I),YSEMI(1,I),NLINES,ZOUT,TEMP1,NZ,0)
CALL UD0322 (ZSEMI(1,I),NLINES,ZOUT,TEMP2,NZ,0)
DO 1160 J=1,NZ
XSEMI(J,I)=TEMP1(J)
YSEMI(J,I)=TEMP2(J)
DO 1420 J=1,NZ
RUS=SQRT((XS(J,1)-YP(J,1))**2+(YS(J,1)-XP(J,1))**2)/2.0
BETA1=ATAN((YS(J,2)+YP(J,1)-YS(J,1))/(XS(J,2)+XP(J,1)-XS(J,1))-XP(J,1))
XINT=AREA*((XP(J,1)+XS(J,1))/2.0-COS(BETA1))*4.0/(3.0*PI)*RD)
YINT=AREA*((YP(J,1)+YS(J,1))/2.0-SIN(BETA1))*4.0/(3.0*PI)*RD)
DO 1170 I=2,NPOINT
DELA=(SQRT((XS(J,I)-XP(J,I))**2+(YS(J,I)-YP(J,I))**2)+SQRT((XS(J,I-1)-XP(J,I-1))**2+(YS(J,I-1)-YP(J,I-1))**2))/4.0
I=I-1
AREA=AREA+DELA
XINT=XINT+DELA
YINT=YINT+DELA
XINT=XINT/AREA
YINT=YINT/AREA
XI=(XS(J,1)+XP(J,1))/2.
YI=(YS(J,1)+YP(J,1))/2.
I1=SQRT((XS(J,1)-XP(J,1))**2+(YS(J,1)-YP(J,1))**2)
F=0.
DO 1180 I=2,NPOINT
I2=SQRT((XS(J,I)-XP(J,I))**2+(YS(J,I)-YP(J,I))**2)

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1180      X2=(XS(J,I)+XB(J,I))/2.
      Y2=(YS(J,I)+YB(J,I))/2.
      CELU=SQRT((X2-X1)**2+(Y2-Y1)**2)
      U=LU+CELU
      IAV3=(I1**3+I2**3)/2.
      F=F+IAV3*CELU
      X1=X2
      Y1=Y2
      I1=I2
      TOPCON=((1./3.)*F)/(1.+(4./3.)*F/AREA/U**2)
      IX=0.0
      IY=0.0
      IXY=0.0
      I=2,4POINT
      XD=SQRT((XS(J,I-1)-XP(J,I-1))**2+(YS(J,I-1)-YP(J,I-1))**2)+SQRT((
      XS(J,I)-XP(J,I))**2+(YS(J,I)-YP(J,I))**2)/2.0
      YD=SQRT((XS(J,I)-XP(J,I))**2+(YS(J,I)-YP(J,I))**2)+SQRT((XP(J
      1,IX)=XD*YD*YD*XD/12.0
      IYD=XD*YD*YD*YD/12.0
      ANG=ATAN((YS(J,I)-YP(J,I)-YP(J,I-1))/(XP(J,I)-XP
      1(J,I-1)-XS(J,I-1)))
      CUSANG=COS(2.0*ANG)
      IXN=(IXU+IYD+(IXU-IYD)*COSANG)/2.0
      IYN=(IXU-IYD-(IXU-IYD)*COSANG)/2.0
      IF (ANG.NE.0.0) IXYN=((IXN-IYJ)*CCSANG-IXU+IYD)/(2.0*SIN(2.0*ANG))
      XLA=XD*YD
      YLN=(YS(J,I)+XS(J,I-1)+YP(J,I-1))/4.0-YINT
      XMN=(XS(J,I)+XP(J,I)-XP(J,I-1))/4.0-YINT
      IX=IX+IXN+DELTA*XMN*YMN
      IY=IY+IYN+DELTA*XMN*XMN
      ANG=ATAN(12.0*(IXY/(IY-IX)))
      IPY=(IX+IY)/2.0+(IX-IY)/2.0*COS(ANG)-IXY*SIN(ANG)
      ANG=ANG/2.0*PI
      IF (IPRINT.EQ.2) 1.02,IPRINT,0.3) GO TO 1325
      IF (LNGT.LT.45) GO TO 1200
      WRITE(LDG2,200)
      LNCT=1
      LNCT=LNCT+16
      WRITE(LDG2,1210) J,ZOUT(J),AREA,XINT,YINT,IX,IY,IPX,ANG,IFY,A
      1V6
      1210      FORMAT(2X,/,30X,14HSECTION NUMBER,13,3X,5H(22,F9.4)/250X,34H**
      12HSECTION AREA,26X,1H=,1P12.4,/,20X,16HSECTION OF PROPERTIES,7X,1
      34HXBAR,3X,1H=,E12.4,/,45X,22HLOCATION OF CENTROID,11X,1$AB
      5H=,E12.4,/,32X,22HSECOND MOMENTS OF AREA,9X,2HIX,5X,1H=,E12.4,
      35X,14H3OUT 3IN,17X,2HIX,5X,1H=,E12.4,/,75X,3HIXY,4X,1H=,F12.

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1350      GO 1350 I=2,31
      XPLOT=XSEMI(J,I)*SCALE
      YPLOT=YSEMI(J,I)*SCALE
      CALL PLOT(XPLOT,YPLOT,2)
      XPLOT=XS(J,I)*SCALE
      YPLOT=YS(J,I)*SCALE
      CALL PLOT(XPLOT,YPLOT,2)
      GO TO 1420
1360      CALL SYMBCL (19.3,2.0,.175,22HCARTESIAN SECTION NO. ,J.0,22)
      X=J
      CALL NUMBER (23.7,2,.,.172,XJ,0.0,-1)
      CALL SYMBOL (20.5,1.0,.,.172,1CHSTAGGER = ,0.0,10)
      STAGGER=ATAN((YS(J,NPOINT)+YP(J,NPOINT))-YS(J,1)-YP(J,1))/(XS(J,NPOINT)-XS(J,1))+C1
1      CALL PLOT (22.35,1,.,.175,STAGGER,0.0,3)
      CALL PLOT (22.0,2,25,-3)
      COSSTG=SIGN(STAGGER/C1)
      YPLOT=75*SINSTG/COSSTG
      XPLOT=4.75*SINSTG/COSSTG
      IF (ABS(XPLOT).LE.22.0) GO TO 1370
      YPLOT=22.0/SINSTG*COSSTG
      CALL PLOT(XPLOT,YPLOT,3)
      XPLOT=-XPLOT
      YPLOT=-YPLOT
      CALL PLOT(XPLOT,YPLOT,2)
      XPLOT=22.0
      YPLOT=22.0*SINSTG/COSSTG
      IF (ABS(YPLOT).LE.4.75) GO TO 1390
      YPLOT=-75/SINSTG*COSSTG
      XPLOT=4.75/SINSTG*COSSTG
      CALL PLOT(XPLOT,YPLOT,3)
      XPLOT=-XPLOT
      YPLOT=-YPLOT
      CALL PLOT(XPLOT,YPLOT,2)
      XPLOT=XPLOT
      YPLOT=XPLOT
      YPLOT=SCALE*(XS(J,I)*COSSTG+YS(J,I)*SINSTG)
      XPLOT=SCALE*(YS(J,I)*COSSTG-XS(J,I)*SINSTG)
      CALL PLOT(XPLOT,YPLOT,3)
      GO 1390 I=2,NPOINT
      YPLOT=SCALE*(XS(J,I)*COSSTG+YS(J,I)*SINSTG)
      XPLOT=SCALE*(YS(J,I)*COSSTG-XS(J,I)*SINSTG)
      CALL PLOT(XPLOT,YPLOT,2)
      GO 1400 I=1,I=NPOINT+1
      XPLOT=SCALE*(XP(J,I)*COSSTG+YP(J,I)*SINSTG)
      YPLOT=SCALE*(YP(J,I)*COSSTG-XP(J,I)*SINSTG)
      CALL PLOT(XPLOT,YPLOT,2)
      GO 1410 I=2,31
      XPLOT=SCALE*(XSEMI(J,I)*COSSTG+YSEMI(J,I)*SINSTG)

```



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1540      FORMAT (4HGOI),IX,I3,AX,SF8.4)
      JD=0
      DO 1550 J=1,NLINES
      DO 1550 I=IRL,IRT
      JD=J)+1
      WRITE (LOG3,1540) JD,XCAMB(J,I),VCMB(J,I),ZCAMB(J,I)
      CONTINUE
      IF (IFPLOT.NE.0) CALL PLOT (0.0,0.0,-3)
      END
1550
1560

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[illegible]

[illegible]

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[illegible]

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SUBROUTINE UJ322 (XDATA,YDATA,NDATA,XI,YOUT,VXY,NTYPE)
DIMENSION XD(1),YD(1),XIN(1),YOUT(1)
CALL UJ327 (XDATA,YDATA,NDATA,XIN,YOUT,XI,XI,VXY,NTYPE,J)
RETURN
END

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[illegible]

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10 SUBROUTINE U0324 (ISTAK,PLISZE,IIRIG,TITLE,IKDUM,IFPLOT)
   DIMENSION TITLE(4)
   IF (IIRIG.EQ.0.AND.IF'LOT.NC.2) CALL PLOT (PLISZE,0.,-3)
   PLT TIT=PLISZE+1 GO TO 10
   IF (ISTAK.LT.2)
     BALE=.35*PLISZE
     XLEN1=.5*PLISZE
     XLEN2=XLEN1
     YLEN1=.25*PLISZE
     YLEN2=-1.*YLEN1
     XBACK1=-1.2
     XBACK2=-5.2
     GO TO 50
   IF (ISTAK.EQ.0) GO TO 20
   XLEN1=.70*PLISZE
   XLEN2=.15*PLISZE
   XBACK1=-1.4-.20*PLISZE
   XBACK2=-5.2-.20*PLISZE
   IF (IKDUM.EQ.1) GO TO 30
   GO TO 40
20 CONTINUE
   XLEN1=.15*PLISZE
   XLEN2=.70*PLISZE
   XBACK1=-1.9+.20*PLISZE
   XBACK2=-5.2+.30*PLISZE
   IF (IKDUM.EQ.1) GO TO 40
   BALE=.25*PLISZE
   YLEN1=.20*PLISZE
   YLEN2=-.15*PLISZE
   GO TO 50
   BALE=.20*PLISZE
   YLEN1=.15*PLISZE
   YLEN2=-.30*PLISZE
30 CONTINUE
   XBACK1=-1.35+BALE
   XBACK2=XBACK1-.01*PLISZE-.175
   CALL PLOT (0.0,-PLISZE,-3)
   CALL PLOT (7.0,PLT TIT,-3)
   CALL PLOT (0.0,BAL,3)
   CALL PLOT (XLEN1,BAL,-2)
   CALL PLOT (XLEN2,0.0,2)
   CALL PLOT (0.0,YLEN1,3)
   CALL PLOT (0.0,YLEN2,2)
   GO TO (10,70), IIRIG
   GO TO SYMCL (XBACK1,XBACK1+.0,3)
   GO TO SYMCL (XBACK1,XBACK1+.175,22HSTPEA4SURFACE SECTIONS,0.0,22)
70 XBACK1=XBACK1+.35
   CALL SYMCL (XBACK1,XBACK1+.175,1HHCARTESIAN SECTIONS,0.0,18)
80 CALL SYMCL (XBACK2,XBACK2+.175,TITLE,0.0,72)
   RETURN

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END

\$245 52

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SUBROUTINE U0327 (XDATA,YDATA,NDATA,XIN,YOUT,SLOPE,YINT,NXY,NTYPE
1,NWOT)
2,CAL N,INT XDATA(1),YDATA(1),XIN(1),YOUT(1),YINT(1),SLOPE(1)
3,DIMENSION M(100),A(100),E(100),INT(100),U(100)
4,N=NDATA-1
5,IF (NTYPE).EQ.0.0,NDATA,SE.3) GO TO 1-0
6,IF (NDATA,ST.1) GO TO 2-0
7,IF (NWOT,GT.3) GO TO 2-0
8,GO 10 I=1,NXY
9,YOUT(I)=YDATA(1)
10,IF (NWOT+NWOT,NE.1) RETURN
11,GO 30 I=1,NXY
12,SLOPE(I)=0.0
13,RETURN
14,IF (NDATA,ST.2) GO TO 8-0
15,YPRIME=(YDATA(12)-YDATA(1))/(XDATA(2)-XDATA(1))
16,IF (NWOT,GT.3) GO TO 5-0
17,GO 50 I=1,NXY
18,YOUT(I)=YDATA(1)+YPRIME*(XIN(I)-XDATA(1))
19,IF (NWOT+NWOT,NE.1) RETURN
20,GO 70 I=1,NXY
21,SLOPE(I)=YPRIME
22,RETURN
23,JE=2
24,GO 130 I=1,NXY
25,IF (XIN(I).LE.XDATA(2)) GO TO 11-0
26,IF (XIN(I).GE.XDATA(N)) GO TO 12-0
27,IF (XIN(I).GE.XDATA(J).AND.XIN(I).LE.XDATA(J+1)) GO TO 10-0
28,JE=J+1
29,IF (J,LE,N-1) GO TO 2-0
30,JE=2
31,GO TO 3-0
32,YOUT(I)=YDATA(J)+(YDATA(J+1)-YDATA(J))/(XDATA(J+1)-XDATA(J))*(XIN
33,I)-XDATA(J))
34,GO TO 13-0
35,YOUT(I)=YDATA(1)+(YDATA(2)-YDATA(1))/(XDATA(2)-XDATA(1))*(XIN(I)-X
36,DATA(1))
37,GO TO 13-0
38,YOUT(I)=YDATA(N)+(YDATA(NDATA)-YDATA(N))/(XDATA(NDATA)-XDATA(N))*
39,XIN(I)-XDATA(N))
40,CONTINUE
41,RETURN
42,A(1)=1.0
43,G(1)=0.0
44,E(1)=0.0
45,GO 150 I=2,N
46,A(I)=(XDATA(I+1)-XDATA(I-1))/3.0-(XDATA(I)-XDATA(I-1))/(6.0
47,*(I-1))
48,A(I)=(XDATA(I+1)-XDATA(I))/6.0
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150  D(I)=(YDATA(I+1)-YDATA(I))/(XDATA(I+1)-XDATA(I))-YDATA(I)-YDATA(I)-YDATA(I)
1  M(XDATA)=0.0
C 160  II=1,N
I=NDATA-II
Y(I)=(D(I))-H(I)*M(I+1))/A(I)
ASSIGN 240 TO L1
ASSIGN 270 TO L2
ASSIGN 290 TO L3
IF (NMOT*EQ(J)) GO TO 190
IF (NMOT*WGT.NE.1) GO TO 170
ASSIGN 260 TO L2
IF (NMOT*EQ(J)) GO TO 190
ASSIGN 230 TO L1
GO TO 190
ASSIGN 230 TO L1
ASSIGN 240 TO L3
INT(I)=0.0
DO 180 J=2,N
X=XDATA(J)-XDATA(J-1)
INT(J)=INT((M(J)+M(J-1))/2+.0*DX*3+DX/2.0*(YDATA(J)+YDATA(J-1)-DX*2*(M(J)+M(J-1))/6.0)
J=1
DO 290 I=1,N
XIN(I)=XDATA(I) GO TO 210
IF (XIN(I).GT.XDATA(I)) GO TO 220
IF (XIN(I).GE.XDATA(J).AND.XIN(I).LE.XDATA(J+1)) GO TO 230
J=J+1
IF (J.L.N) GO TO 200
J=1
GO TO 200
YPRIME=(M(2)/3+H(1)/3.0)*(XDATA(1)-XDATA(2))+(YDATA(2)-YDATA(1))
1/(XDATA(2)-XDATA(1))
IF (NMOT*LE.1) YOUT(I)=YDATA(1)+YPRIME*(XIN(I)-XDATA(1))
IF (NMOT*WGT.EQ.1) SLOPE(I)=YPRIME
GO TO 290
YPRIME=(M(NDATA)/3.0+M(N)/6.0)*(XDATA(NDATA)-XDATA(N))+YDATA(NDATA)
1/(XDATA(N)-XDATA(N))
IF (NMOT*LE.1) YOUT(I)=YDATA(NDATA)+YPRIME*(XIN(I)-XDATA(NDATA))
IF (NMOT*WGT.EQ.1) SLOPE(I)=YPRIME
GO TO 290
DX=XDATA(J+1)-XDATA(J)
GO TO L1
YOUT(I)=Y(J)/(6.0*DX)*(XDATA(J+1)-XIN(I))+3*(Y(J+1)/(5.0*DX)*(XIN(I)-XDATA(J+1)-XIN(I))+YDATA(J)/DX-M(J)/6.0*DX)
1/(XDATA(J)-XDATA(J))+3*(XDATA(J+1)-XDATA(J))/6.0*DX
GO TO L2
GO TO L2
SLOPE(I)=(-M(J)*(XDATA(J+1)-XDATA(J))+2/2.0*M(J+1)*(XIN(I)-XDATA(J)+2/2.0*YDATA(J+1)-YDATA(J))/DX-M(J+1)-M(J))/6.0*DX
GO TO 290

```



```

270      GO TO L5, (2), (290)
280      YINT(I)=INT(J)-4(J)/(24.0*UX)*(XDATA(J+1)-XIN(I))*4+Y(J+1)/(24.0*
      10X)*(XIN(I)-XDATA(J))/DX-M(J)/6.0*UX)*(XDATA(J+1)-XIN(I))*2/2.0
      2(I))*2/2.0+(YDATA(J+1)/DX-4(J+1)/6.0*UX)*(XIN(I)-XDATA(J))*2/2.0
      3+M(Y)/2.0*UX*3+(YDATA(J)-M(J)/5.0*UX*2)*DX/2.0
      404TIME
      RETURN
      END
102
103
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105
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```

SECTION II

EXAMPLES OF USE OF PROGRAM

1. DISCUSSION OF EXAMPLE A

The example shown is the design of a single-stage compressor and is based upon a design described in Reference 1. The input data cards are shown in the next subsection, and selected output data are shown in the following subsection. An analytic meanline rotor blade and an arbitrary meanline stator are used, so that with the aerodynamic calculations all three program sections are used.

The original design was made using 15 streamsurfaces to describe the flow, but in the interests of economy, only 8 have been used here. The same computing station geometry is used here as was used in the original design, and alternate streamsurfaces, as derived previously, are input to the analytic meanline section for the rotor geometry determination. Streamsurfaces are specified from one station upstream of the leading edge to one station downstream of the trailing edge. Blade section specifications were also reproduced directly, and these specify a polynomial camberline blade with an uncambered leading edge. Output of NASTRAN data cards is specified by setting INAST = 4. Thus four-point averaging will be used, and no pressure load cards will be punched. Input to the interface routine includes a shape correction factor of 0.7, and a single deviation fraction curve, as was used originally. One degree of additional deviation at the trailing edge (over that determined by the basic deviation rule) is specified, and the point of maximum camber is given as 0.75 of the blade chord. The loss form indicator NLOSS is set to 4 for each station within the rotor blade, so that (in the aerodynamic analysis) loss coefficients will be determined as a function of the trailing edge values. Accordingly, NLOSS is set to 1 for the trailing edge, and a loss coefficient distribution is given. The results show the blade inlet, outlet, and camber angles as positive; they are set positive in this routine so that they may be used in conjunction with the deviation rule data. The additional deviation remains positive, but the total deviation is shown negative, as it is used in the aerodynamic section in conjunction with (generally) negative rotor blade angles.

The input printout from the aerodynamic section follows, and it is seen that blade geometry for stations 4 through 9 are to come internally from the analytic meanline section. These data are listed with the rest, and show, for stations 5 through 9, the deviation "rising" from about -1.5 degrees to the trailing edge values of about -13.5 degrees. No loss

coefficients are shown for stations 5 through 8; these will be generated internally from values at station 9, and the loss fraction curve shown as the final input data. A simple linear increase from leading edge to trailing edge is indicated. For the stator, whirl velocity is specified and NOUT2 is set to 1 from one station upstream of the bladerow to one station downstream. Thus data will be output for the arbitrary meanline blade section. For each of the stations within the stator, an isentropic efficiency variation is given, relative to conditions at the rotor inlet. At the trailing edge, a relative total pressure loss coefficient is given, because for both rotor and stator a loss re-estimation is specified. As NEVAL is negative for stations 9 and 15, the new losses will not be incorporated into the iteration, but will be computed after the solution is converged. One family of loss parameter/diffusion factor curves is given in the data, and is called out for both blades. For the rotor, NDEL is set to 2, and the specified Prandtl-Meyer expansion angle varies from zero at the hub to -5 degrees (that is, 5 degrees of compression) at the tip. As leading edge geometry is given, the incidence angles will be added to these values. NDEL is set to zero for the stator, so that no shock loss will be computed. Pressure load cards for the NASTRAN program are specified for both rotor and stator. Four-point averages are specified for the rotor, three-point for the stator.

The output from aerodynamic analysis shows details of the flow through the machine, and is very similar to that shown in Reference 1. The loss coefficient re-estimation shows a relatively high rotor loss coefficient, due principally to a less optimistic assumption regarding precompression of the inlet flow.

The stator blade design follows, producing a blade that corresponds to the air angle distribution determined through it in the aerodynamic section. A uniform 3 degrees of incidence and 1 degree of extra deviation are specified. INAST is set to -3, specifying the output of NASTRAN data cards for the stator, without pressure load cards (which are specified for the aerodynamic section). Three-point averages are to be used. Details of the resulting blade section for the innermost streamsurface are shown.

2. INPUT DATA CARD LISTING FOR EXAMPLE A

The input data cards are shown on the following pages, 50 cards per page. No completely blank cards have been used.

0.00695	260.0	.875	0.0	.08	DATA1253
0.002508	268.0	.854	0.0	.08	DATA1254
0.00345	292.0	.820	0.0	.04	DATA1255
0.005632	327.0	.761	0.0	.03	DATA1256
0.00000	0	0	0	0	DATA1257
0.00000	0	0	0	0	DATA1258
0.00000	0	0	0	0	DATA1259
0.00000	0	0	0	0	DATA1260
0.00000	0	0	0	0	DATA1261
0.00000	0	0	0	0	DATA1262
0.00000	0	0	0	0	DATA1263
0.00000	0	0	0	0	DATA1264
0.00000	0	0	0	0	DATA1265
0.00000	0	0	0	0	DATA1266
0.00000	0	0	0	0	DATA1267
0.00000	0	0	0	0	DATA1268
0.00000	0	0	0	0	DATA1269
0.00000	0	0	0	0	DATA1270
0.00000	0	0	0	0	DATA1271
0.00000	0	0	0	0	DATA1272
0.00000	0	0	0	0	DATA1273
0.00000	0	0	0	0	DATA1274
0.00000	0	0	0	0	DATA1275
0.00000	0	0	0	0	DATA1276
0.00000	0	0	0	0	DATA1277
0.00000	0	0	0	0	DATA1278
0.00000	0	0	0	0	DATA1279
0.00000	0	0	0	0	DATA1280
0.00000	0	0	0	0	DATA1281
0.00000	0	0	0	0	DATA1282
0.00000	0	0	0	0	DATA1283
0.00000	0	0	0	0	DATA1284
0.00000	0	0	0	0	DATA1285
0.00000	0	0	0	0	DATA1286
0.00000	0	0	0	0	DATA1287
0.00000	0	0	0	0	DATA1288
0.00000	0	0	0	0	DATA1289
0.00000	0	0	0	0	DATA1290
0.00000	0	0	0	0	DATA1291
0.00000	0	0	0	0	DATA1292
0.00000	0	0	0	0	DATA1293
0.00000	0	0	0	0	DATA1294
0.00000	0	0	0	0	DATA1295
0.00000	0	0	0	0	DATA1296
0.00000	0	0	0	0	DATA1297
0.00000	0	0	0	0	DATA1298
0.00000	0	0	0	0	DATA1299
0.00000	0	0	0	0	DATA1300
0.00000	0	0	0	0	DATA1301

3. SELECTIONS FROM OUTPUT DATA FOR EXAMPLE A

0.0000	6.7546	1	6.7545	-0.0000
0.0000	A.9900	2	7.0473	-0.0000
		3	7.3793	-0.0000
		4	7.6339	-0.0000
		5	A.2222	-0.0000
		6	A.7473	-0.0000
		7	A.6555	-0.0000
		8	A.9900	-0.0000

COMPUTING STATION 3 NUMBER OF DESCRIBING POINTS= 2 IFANGS(3)= 1

DESCRIPTION R STREAMLINE NUMBER RADIUS DELTA PRESSURE

0.000	7.0471	1	6.0064	-0.0000
0.000	7.0471	2	7.0471	-0.0000
		3	7.0471	-0.0000
		4	7.0471	-0.0000
		5	7.0471	-0.0000
		6	7.0471	-0.0000
		7	7.0471	-0.0000
		8	7.0471	-0.0000
		9	7.0471	-0.0000

COMPUTING STATION 4 NUMBER OF DESCRIBING POINTS= 2 IFANGS(4)= 1

DESCRIPTION R STREAMLINE NUMBER RADIUS DELTA PRESSURE

0.000	7.0471	1	7.0471	-0.0000
0.000	7.0471	2	7.0471	-0.0000
		3	7.0471	-0.0000
		4	7.0471	-0.0000
		5	7.0471	-0.0000
		6	7.0471	-0.0000
		7	7.0471	-0.0000
		8	7.0471	-0.0000
		9	7.0471	-0.0000

COMPUTING STATION 5 NUMBER OF DESCRIBING POINTS= 2 IFANGS(5)= 1

DESCRIPTION R STREAMLINE NUMBER RADIUS DELTA PRESSURE

1.200	7.0471	1	7.0471	-0.0000
1.200	7.0471	2	7.0471	-0.0000
		3	7.0471	-0.0000
		4	7.0471	-0.0000
		5	7.0471	-0.0000
		6	7.0471	-0.0000
		7	7.0471	-0.0000
		8	7.0471	-0.0000
		9	7.0471	-0.0000

IFANGS(6) = 1

COMPUTING STATION 6		NUMBER OF DESCRIBING POINTS = 2		IFANGS(6) = 1	
DESCRIPTION X	STREAMLINE NUMBER	RANT	DELTA PRESSURE		
1.6000	7.6479	7.6479	-2.0000		
1.6000	8.7224	7.6395	-0.0000		
		7.7047	-0.0000		
		7.9642	-0.0000		
		8.1417	-0.0000		
		8.3241	-0.0000		
		8.5146	-0.0000		
		8.7225	-0.0000		

IFANGS(7) = 1

COMPUTING STATION 7		NUMBER OF DESCRIBING POINTS = 2		IFANGS(7) = 1	
DESCRIPTION X	STREAMLINE NUMBER	RANT	DELTA PRESSURE		
2.0000	7.5545	7.5545	-0.0000		
2.0000	8.6556	7.6464	-0.0000		
		7.9247	-0.0000		
		7.9720	-0.0000		
		8.1285	-0.0000		
		8.2044	-0.0000		
		8.4247	-0.0000		
		8.6556	-0.0000		

IFANGS(8) = 0

COMPUTING STATION 8		NUMBER OF DESCRIBING POINTS = 2		IFANGS(8) = 0	
DESCRIPTION X	STREAMLINE NUMBER	RANT	DELTA PRESSURE		
2.3000	7.5460	7.5460	-0.0000		
2.3000	8.6279	7.7078	-0.0000		
		7.8134	-0.0000		
		7.9737	-0.0000		
		8.1271	-0.0000		
		8.2924	-0.0000		
		8.4459	-0.0000		
		8.6279	-0.0000		

DEVIATION FRACTION CURVES AT 1 RADII

RTF = 3.0000

DM
 DVF0AC
 0.0000
 .1000
 .2000
 .3000
 .4000
 .5000
 .6000
 .7000
 .8000
 .9000
 1.0000

WJF
 DELTAN
 AC
 3.0000
 1.00
 .7500

RESULTS

STREAMLINE	RTA1	RTA2	CAMPEP	T/C	A/C	SOLIDITY	ADDT. DEVM	TOTAL DEVIATION
1	41.543	17.455	49.094	.0444	.7500	2.17139	1.0000	-13.7617
2	61.475	15.444	46.150	.0454	.7500	2.07929	1.0000	-13.3976
3	62.152	14.214	43.924	.0424	.7500	2.03944	1.0000	-13.344
4	62.628	20.162	42.266	.0506	.7500	1.95734	1.0000	-12.8490
5	63.179	21.875	41.104	.0372	.7500	1.91930	1.0000	-12.8050
6	63.791	23.147	40.559	.0351	.7500	1.89204	1.0000	-12.7750
7	64.180	24.083	40.127	.0332	.7500	1.87245	1.0000	-12.7943
8	64.705	24.317	40.184	.0313	.7500	1.85988	1.0000	-12.9930

STATION 3 NUMBER OF RADII= 4			
RADIUS	SECTION ANGLE	LEAN ANGLE	BLADE BLOCKAGE THETA
6.9246	-60.4939	10.9559	.1218
7.1971	-61.9813	7.9964	.1130
7.4826	-61.1324	6.6181	.1052
7.7611	-61.3769	3.1169	.0923
8.0537	-61.7154	1.9103	.0883
8.3477	-62.0171	1.2256	.0814
8.6296	-62.2771	1.2549	.0773
8.9231	-61.5906	1.3787	.0741

STATION 4 NUMBER OF RADII= 5			
RADIUS	SECTION ANGLE	LEAN ANGLE	BLADE BLOCKAGE THETA
7.1871	-55.8167	4.6139	.1628
7.3579	-56.6217	1.7534	.1468
7.6234	-56.5214	-0.6660	.1342
7.8084	-56.7717	-0.8427	.1241
8.1354	-56.9127	-0.9722	.1164
8.4563	-57.4493	-0.4471	.1132
8.6710	-58.1541	1.0131	.1049
8.9562	-59.0908	2.9254	.1033

STATION 5 NUMBER OF RADII= 4			
RADIUS	SECTION ANGLE	LEAN ANGLE	BLADE BLOCKAGE THETA
7.1277	-68.1715	-6.4963	.1431
7.3241	-67.0589	-5.9879	.1296
7.7262	-65.8303	-4.8216	.1194
7.9372	-67.1644	-5.8476	.1116
8.1374	-67.9216	-2.1974	.1054
8.7644	-68.8516	-1.8097	.1003
8.5649	-69.1304	1.4679	.0957
8.7894	-50.7842	3.6429	.0910

RADIUS	STATION 6				THETA
	SECTION ANGLE	LEAH ANGLE	BLADE BLOCKAGE		
7.6479	-29.7797	-9.7012	.0944		-.0962
7.6306	-31.0116	-6.4785	.0888		-.0936
7.7987	-32.0247	-3.6480	.0828		-.0915
7.7542	-33.4940	-1.7777	.0760		-.0916
7.8117	-34.8749	.0125	.0739		-.0915
7.8251	-36.2126	1.2402	.0757		-.0918
7.8166	-37.1719	2.2186	.0668		-.0915
7.7255	-38.2360	3.1126	.0631		-.0927

RADIUS	STATION 7				THETA
	SECTION ANGLE	LEAH ANGLE	BLADE BLOCKAGE		
7.6695	-12.7527	-3.3125	.0332		-.1151
7.6446	-15.2054	.1571	.0306		-.1146
7.8243	-17.3746	2.0667	.0291		-.1150
7.8770	-20.1786	2.5614	.0262		-.1158
7.8246	-21.7647	3.2022	.0246		-.1169
7.8916	-23.1637	3.4969	.0233		-.1181
7.8667	-24.2135	3.2060	.0221		-.1192
7.8556	-24.6056	2.6098	.0210		-.1203

DEVIATION FRACTION CURVES AT 1 RADII

RTF = 3.0000

RTF	DELTA	AC
0.0000	1.000	.7500
.2500		
.5000		
.7500		
1.0000		

RESULTS

STREAMLINE	RTA1	RTA2	CALC	T/C	A/C	SOLIDITY	ADDT. DEVM	TOTAL DEVIATION
1	41.543	17.455	49.004	.044	.7500	2.12139	1.0000	-13.7617
2	61.826	15.444	44.150	.044	.7500	2.07929	1.0000	-13.3976
3	62.152	14.218	43.924	.042	.7500	2.03944	1.0000	-13.144
4	62.628	20.162	42.266	.036	.7500	1.95734	1.0000	-12.8490
5	63.179	21.875	41.304	.032	.7500	1.92930	1.0000	-12.9050
6	63.701	23.147	40.559	.031	.7500	1.89204	1.0000	-12.7750
7	64.180	24.087	40.127	.032	.7500	1.87245	1.0000	-12.7943
8	64.705	24.317	40.144	.031	.7500	1.85980	1.0000	-12.9930

SECRET

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STATION & LOCATION
ALUMINUM
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YSTU BOSTON
-1-3093 6-1766
\$30.00

ATION 3 SPECIFIED BY 2 POINTS

0350.0	0059.0
0350.0	0059.0
0350.0	0059.0

STATION 15 NDATA= 4 NTFOR= 0 NDTM= 0 NMACH= 0 NHPK= 4 NLOSS= 1 NL1= -4 NL2= -4 NEVAL= -1 NCURVE= 1 NLITER= 0 NOEL= 0
 NOUT1= 0 NOUT2= 1 NOUT3= 2 NALATE= 49

SPEED = 0.00

DATA0	DATA1	DATA2	DATA3	DATA4	DATA5	DATA6	DATA7	DATA8	DATA9
7.4814	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
7.4817	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
7.4820	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
7.4823	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
7.4826	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
7.4829	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

STATION 16 NDATA= 4 NTFOR= 0 NDTM= 0 NMACH= 0 NHPK= 4 NLOSS= 1 NL1= -3 NL2= -3 NEVAL= -0 NCURVE= -0 NLITER= -0 NOEL= -0
 NOUT1= 0 NOUT2= 1 NOUT3= 2 NALATE= 49

STATION 17 NDATA= 4 NTFOR= 0 NDTM= 0 NMACH= 0 NHPK= 4 NLOSS= 1 NL1= -0 NL2= -0 NEVAL= -0 NCURVE= -0 NLITER= -0 NOEL= -0
 NOUT1= 0 NOUT2= 1 NOUT3= 2 NALATE= 49

BLOCKAGE FACTOR SPECIFICATIONS

STATION WALL BLOCKAGE WAKE BLOCKAGE WAKE DISTRIBUTION FACTOR

STATION	WALL BLOCKAGE	WAKE BLOCKAGE	WAKE DISTRIBUTION FACTOR
15	0.0000	0.0000	0.0000
16	0.0000	0.0000	0.0000
17	0.0000	0.0000	0.0000

LOSS PARAMETER / DIFFUSION FACTOR CURVES FOR BLADE TYPE 1 5 D-FACTORS GIVEN

DIFFUSION FACTOR	L	U	S	D	A	P	M	E	T	E	T	T
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

FRACTIONAL LOSS DISTRIBUTION CURVES FOR BLADE CLASS 1 2 POINTS GIVEN AT 1 RADIAL LOCATIONS

FRACTION OF COMPUTING STATION LENGTH AT PLANE EXIT = 0.000

FRACTION OF COMPUTING STATION LENGTH AT PLANE EXIT = 0.000

FRACTION OF COMPUTING STATION LENGTH AT PLANE EXIT = 0.000

LOSS/LOSS AT TRAILING EDGE

0.000

1.000

PROGRAM HORTON - COMBINATION DESIGN - ARBITRARY MEANLINE BLADE SECTION

TITLE = STATOR BLADE DESIGN

NUMBER OF STREAMSURFACES = 4
 NUMBER OF STATIONS = 7
 NUMBER OF CONSTANT-7 PLANS = 10
 NUMBER OF PLANE DATA POINTS = 1
 NUMBER OF POINTS PER SEGMENT = 15
 NUMBER OF BLADES IN BLADE ROW = 49
 RATIO = 1
 TANGENT = 0
 TANGENT = 0
 TANGENT = -0
 TANGENT = -0
 TANGENT = -3
 TANGENT = 7.5000
 TANGENT = 9.6250
 TANGENT = 1.0000
 TANGENT = 0.0000
 TANGENT = 11.0000

LEADING EDGE STATION NUMBER = 2
 TRAILING EDGE STATION NUMBER = 6
 BLADE COEFFICIENT OF LIFT = 1
 BLADE COEFFICIENT OF DRAG = 1
 BLADE COEFFICIENT OF MOMENT = 1
 BLADE COEFFICIENT OF TORSION = 1

SHAPE FACTOR = .700
 SOLIDITY TOLERANCE = .0100

DEVIATION CURVE 1 NUMBER OF POINTS = 5 RADIUS = 0.0000

POINT	NORMALIZED MECHANICAL CHARGE	NORMALIZED DEVIATION DISTRIBUTION
1	0.0000	.1000
2	.2500	.1100
3	.5000	.1200
4	.7500	.1300
5	1.0000	1.0000

INCIDENCE AND EXTRA DEVIATION DISTRIBUTION

INLET RADIUS	INCIDENCE	EXTRA DEVIATION
0.0000	7.000	1.000

STANDARD SUPPLY COMPANY

COMPUTING STATION 1		NUMBER OF DESCRIBING POINTS= 4	AIR ANGLE	IFANGS(1)= 0
RECROSSITION Y	STRAKLINE NUMBER	RADIUS	DELTA PRESSURE	
7.5442	1	7.5442	53.4168	-0.0000
7.4000	2	7.7140	52.8112	-0.0000
7.4000	3	7.7140	52.8112	-0.0000
7.4000	4	7.7140	52.8112	-0.0000
7.4000	5	7.7140	52.8112	-0.0000
7.4000	6	7.7140	52.8112	-0.0000
7.4000	7	7.7140	52.8112	-0.0000
7.4000	8	7.7140	52.8112	-0.0000
7.4000	9	7.7140	52.8112	-0.0000
7.4000	10	7.7140	52.8112	-0.0000
7.4000	11	7.7140	52.8112	-0.0000
7.4000	12	7.7140	52.8112	-0.0000
7.4000	13	7.7140	52.8112	-0.0000
7.4000	14	7.7140	52.8112	-0.0000
7.4000	15	7.7140	52.8112	-0.0000
7.4000	16	7.7140	52.8112	-0.0000
7.4000	17	7.7140	52.8112	-0.0000
7.4000	18	7.7140	52.8112	-0.0000
7.4000	19	7.7140	52.8112	-0.0000
7.4000	20	7.7140	52.8112	-0.0000
7.4000	21	7.7140	52.8112	-0.0000
7.4000	22	7.7140	52.8112	-0.0000
7.4000	23	7.7140	52.8112	-0.0000
7.4000	24	7.7140	52.8112	-0.0000
7.4000	25	7.7140	52.8112	-0.0000
7.4000	26	7.7140	52.8112	-0.0000
7.4000	27	7.7140	52.8112	-0.0000
7.4000	28	7.7140	52.8112	-0.0000
7.4000	29	7.7140	52.8112	-0.0000
7.4000	30	7.7140	52.8112	-0.0000
7.4000	31	7.7140	52.8112	-0.0000
7.4000	32	7.7140	52.8112	-0.0000
7.4000	33	7.7140	52.8112	-0.0000
7.4000	34	7.7140	52.8112	-0.0000
7.4000	35	7.7140	52.8112	-0.0000
7.4000	36	7.7140	52.8112	-0.0000
7.4000	37	7.7140	52.8112	-0.0000
7.4000	38	7.7140	52.8112	-0.0000
7.4000	39	7.7140	52.8112	-0.0000
7.4000	40	7.7140	52.8112	-0.0000
7.4000	41	7.7140	52.8112	-0.0000
7.4000	42	7.7140	52.8112	-0.0000
7.4000	43	7.7140	52.8112	-0.0000
7.4000	44	7.7140	52.8112	-0.0000
7.4000	45	7.7140	52.8112	-0.0000
7.4000	46	7.7140	52.8112	-0.0000
7.4000	47	7.7140	52.8112	-0.0000
7.4000	48	7.7140	52.8112	-0.0000
7.4000	49	7.7140	52.8112	-0.0000
7.4000	50	7.7140	52.8112	-0.0000
7.4000	51	7.7140	52.8112	-0.0000
7.4000	52	7.7140	52.8112	-0.0000
7.4000	53	7.7140	52.8112	-0.0000
7.4000	54	7.7140	52.8112	-0.0000
7.4000	55	7.7140	52.8112	-0.0000
7.4000	56	7.7140	52.8112	-0.0000
7.4000	57	7.7140	52.8112	-0.0000
7.4000	58	7.7140	52.8112	-0.0000
7.4000	59	7.7140	52.8112	-0.0000
7.4000	60	7.7140	52.8112	-0.0000
7.4000	61	7.7140	52.8112	-0.0000
7.4000	62	7.7140	52.8112	-0.0000

COMPUTING STATION 5 NUMBER OF DESCRIBING POINTS= 4 IFANCS(5)= 0

DESCRIPTION X STOPFRAME NUMBER RATIO AIR ANGLE DELTA PRESSURE

6.172 7.9077 1 7.7077 6.7455 -0.0000
6.173 7.9107 2 7.8159 -0.0000
6.174 7.9107 3 7.915 5.3629 -0.0000
6.175 7.9107 4 8.043 4.3077 -0.0000
6.176 7.9107 5 8.175 4.3443 -0.0000
6.177 7.9107 6 8.312 4.4713 -0.0000
6.178 7.9107 7 8.449 4.5915 -0.0000
6.179 7.9107 8 8.577 4.7042 -0.0000

COMPUTING STATION 6 NUMBER OF DESCRIBING POINTS= 2 IFANCS(6)= 0

DESCRIPTION X STOPFRAME NUMBER RATIO AIR ANGLE DELTA PRESSURE

6.220 7.6419 1 7.6419 0.0000 -0.0000
6.221 7.6419 2 7.7429 0.0000 -0.0000
6.222 7.6419 3 7.8439 0.0000 -0.0000
6.223 7.6419 4 8.017 0.0000 -0.0000
6.224 7.6419 5 8.175 0.0000 -0.0000
6.225 7.6419 6 8.312 0.0000 -0.0000
6.226 7.6419 7 8.449 0.0000 -0.0000
6.227 7.6419 8 8.577 0.0000 -0.0000

COMPUTING STATION 7 NUMBER OF DESCRIBING POINTS= 2 IFANCS(7)= 0

DESCRIPTION X STOPFRAME NUMBER RATIO AIR ANGLE DELTA PRESSURE

6.300 7.6419 1 7.6419 0.0000 -0.0000
6.301 7.6419 2 7.7429 0.0000 -0.0000
6.302 7.6419 3 7.8439 0.0000 -0.0000
6.303 7.6419 4 8.017 0.0000 -0.0000
6.304 7.6419 5 8.175 0.0000 -0.0000
6.305 7.6419 6 8.312 0.0000 -0.0000
6.306 7.6419 7 8.449 0.0000 -0.0000
6.307 7.6419 8 8.577 0.0000 -0.0000

SECTION GEOMETRY SPECIFICATIONS

STOPFRAME NUMBER SOLIDITY MONITOR LE RADIUS /CHORD MAX THICK /CHORD TE THICK /2*CHORD POINT OF MAX THICK X STACK OFFSET Y STACK OFFSET

1.0 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

STOPFRAME SURFACE 1

ITERATION 1 DEVIATION = 9.461 SOLIDITY = 2.5497
ITERATION 2 DEVIATION = 9.460 SOLIDITY = 2.4060
ITERATION 3 DEVIATION = 9.460 SOLIDITY = 2.4060

POINT NO.	STATION M	Y	Y-Q (PFC)	Y-Q	RAO OF CUEV
1	0.0000	0.0000	51.393646	-2.145914	-1.2143
2	0.01787	0.01787	50.11431	-3.127791	-1.0117
3	0.03574	0.03574	49.564335	-3.157751	-1.0020
4	0.05357	0.05357	49.26246	-3.111723	-0.9523
5	0.07143	0.07143	49.196091	-3.256162	-0.8876
6	0.08926	0.08926	49.223726	-3.141281	-0.9332
7	0.10713	0.10713	42.009159	-3.109908	-0.7887
8	0.12500	0.12500	41.009752	-2.947343	-0.7536
9	0.14287	0.14287	38.651727	-2.859477	-0.7280
10	0.16074	0.16074	36.565138	-2.720140	-0.7123
11	0.17861	0.17861	36.976832	-2.764741	-0.7013
12	0.19648	0.19648	37.132970	-2.391711	-0.7141
13	0.21435	0.21435	31.477852	-2.002569	-0.7313
14	0.23222	0.23222	29.462187	-1.997155	-0.7677
15	0.25009	0.25009	29.788574	-1.775312	-0.8273
16	0.26796	0.26796	27.005529	-1.551470	-0.9132
17	0.28583	0.28583	25.971528	-1.167728	-1.0106
18	0.30370	0.30370	24.931640	-1.159816	-1.0448
19	0.32157	0.32157	23.496643	-0.11146	-1.0295
20	0.33944	0.33944	23.40310	-0.97921	-1.0433
21	0.35731	0.35731	22.721179	-0.76099	-1.0489
22	0.37518	0.37518	21.774744	-0.79916	-1.0375
23	0.39305	0.39305	21.166140	-0.513493	-0.9081
24	0.41092	0.41092	20.639410	-0.571803	-2.01336
25	0.42879	0.42879	20.136835	-1.52707	-2.1861
26	0.44666	0.44666	19.076651	-1.566444	-2.1519
27	0.46453	0.46453	18.117074	-0.93101	-2.0331
28	0.48240	0.48240	18.563212	-0.83678	-1.8553
29	0.50027	0.50027	17.966711	-0.705174	-1.6470
30	0.51814	0.51814	17.000711	-0.798215	-1.4516
31	0.53601	0.53601	16.077708	-0.92371	-1.3141
32	0.55388	0.55388	15.074421	-0.92374	-1.2049
33	0.57175	0.57175	14.716823	-0.947035	-1.1108
34	0.58962	0.58962	13.743616	-1.036366	-1.0528
35	0.60749	0.60749	12.718131	-1.07170	-1.0012
36	0.62536	0.62536	11.647718	-1.00914	-0.9404
37	0.64323	0.64323	11.564147	-1.133335	-0.9285
38	0.66110	0.66110	9.41074	-1.169725	-0.9046
39	0.67897	0.67897	8.209103	-1.155651	-0.9046
40	0.69684	0.69684	7.007101	-1.154366	-0.8928
41	0.71471	0.71471	5.970642	-1.147398	-0.8867
42	0.73258	0.73258	4.974617	-1.125648	-0.8883
43	0.75045	0.75045	4.053311	-1.098415	-0.9979
44	0.76832	0.76832	2.647729	-1.067337	-0.9195
45	0.78619	0.78619	1.471616	-1.039120	-0.9614
46	0.80406	0.80406	0.422609	-1.011778	-0.9875
47	0.82193	0.82193	-0.611122	-0.988741	-1.0116
48	0.83980	0.83980	-1.601197	-0.967030	-1.0353
49	0.85767	0.85767	-2.570743	-0.947635	-1.0749
50	0.87554	0.87554	-3.538855	-0.930464	-1.0869
51	0.89341	0.89341	-4.476624	-0.915509	-1.1022
52	0.91128	0.91128	-5.399882	-0.903765	-1.1222
53	0.92915	0.92915	-6.310486	-0.892756	-1.1467
54	0.94702	0.94702	-7.200718	-0.884757	-1.1755
55	0.96489	0.96489	-8.091222	-0.879043	-1.1723
56	0.98276	0.98276	-8.984896	-0.875613	-1.1850
57	1.00063	1.00063	-9.8861071	-0.874673	-1.1955

DATA POINTS

1	0.00000	51.399644
2	0.01123	29.146977
3	0.02246	17.872852
4	0.03369	8.577609
5	0.04492	-9.860073

STREAMSURFACE GEOMETRY ON STREAMLINE NUMBER 1 *****

RY11 = 51.309 (PLANE INLET ANGLE.)
 RY12 = -9.840 (PLANE OUTLET ANGLE.)
 RY13 = 1.0500 (PLANE LEADING EDGE RADIUS AS A FRACTION OF CHORD.)
 RY14 = 1.5100 (PLANE MAXIMUM THICKNESS AS A FRACTION OF CHORD.)
 RY15 = 1.0500 (PLANE TRAILING EDGE HALF-THICKNESS AS A FRACTION OF CHORD.)
 RY16 = 1.7020 (LOCATION OF MAXIMUM THICKNESS AS A FRACTION OF MEAN LINE.)
 RY17 = 2.2272 (MEDIAN CHORD OF SECTION.)

NORMALIZED RESULTS - ALL THE FOLLOWING REFER TO AIRLAGE HAVING A MERIDIONAL CHORD PROJECTION OF UNITY

RL OF CHORD = 1.0595

STAGGED ANGLE = 19.487

CAMBER ANGLE = 61.240

SECTION AREA = .05002

LOCATION OF CENTROID RELATIVE TO LEADING EDGE

XBAR = .52189
 YBAR = .27204

SECOND MOMENTS OF AREA ABOUT CENTROID

IXX = .00319
 IYY = .00115
 IXY = .00100

ANGLE OF INCLINATION OF (ONE) PRINCIPAL A.XIS TO (XC AXIS) = 17.867

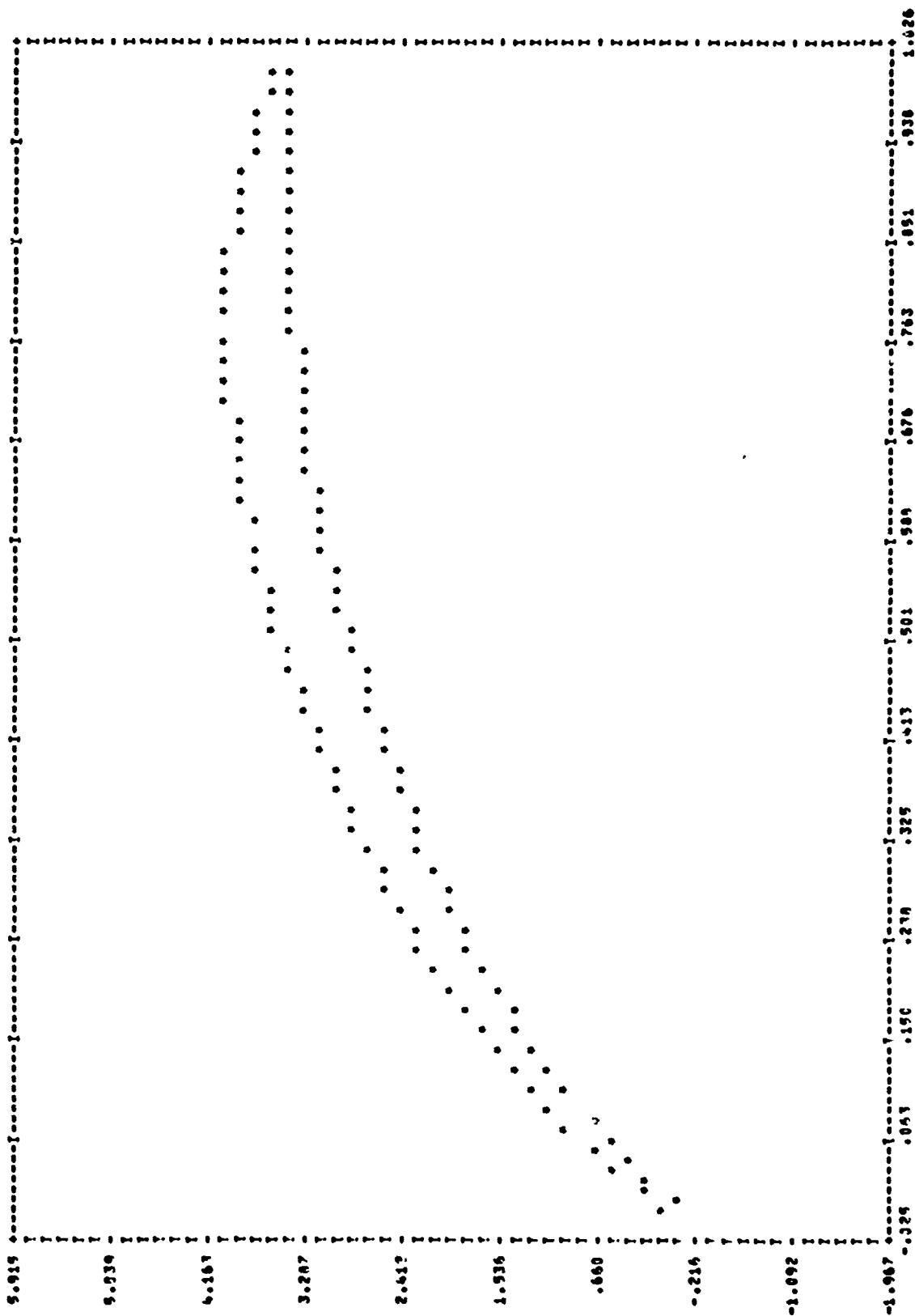
PRINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROID

I1X = .00304 (AT 17.867 WITH (XC AXIS))
 I1Y = .00347 (AT 17.867 WITH (XC AXIS))

POINT NUMBER	X	Y	H	A	L	T	A	ANGLE THICKNESS	SURFACE COORDINATE DATA			
									X1	Y1	X2	Y2
1	.00000	.00000	51.309	1.059	.01059				.00115	.00330	.00944	-.00330
2	.02804	.02169	51.312	.01347					.01744	.02602	.02820	.01737
3	.06079	.06332	68.564	.01424					.03471	.06370	.04888	.03694
4	.05844	.14194	47.074	.01804					.03163	.06834	.04547	.03542
5	.37428	.08170	45.397	.02154					.04841	.07796	.04336	.07282
6	.06003	.09797	43.726	.02474					.04571	.11657	.11235	.08918
7	.11174	.14354	42.012	.02644					.12292	.12418	.12063	.10432
8	.12052	.12945	40.239	.02477					.13224	.14081	.13882	.11884
9	.16727	.14440	38.461	.03099					.17763	.15653	.15491	.13226
10	.16501	.15904	36.456	.03112					.15513	.17133	.17490	.14476
11	.18776	.17083	34.876	.03454					.17271	.18325	.19281	.15640
12	.20351	.18280	33.133	.03712					.19036	.19734	.21005	.16726
13	.21425	.19401	31.453	.03900					.20804	.21064	.22843	.17736

NORMALISED PLOT OF SECTION NUMBER 1

SCALES - (X) IS SHOWN TIMES .0 TO THE POWER OF -3 (Y) IS SHOWN TIMES 10 TO THE POWER OF 1



DIMENSIONAL RESULTS - ALL RESULTS REFER TO A BLADE OF SPECIFIED CHORD

PLANFORM CHORD = 2.3770E+00

L.F. RADIUS = 1.1797E-02

SECTION AREA = 2.4766E-01

SECOND MOMENTS OF AREA ABOUT CENTROID

IX = 0.4777E-01

IY = 7.2127E-02

IYY = 2.4100E-02

PRINCIPAL SECOND MOMENTS OF AREA ABOUT CENTROID

IPV = 1.5641E-01 (AT 17.467 WITH CVC AXIS)

IPV = 8.6183E-02 (AT 17.467 WITH CVC AXIS)

PT NO	SURFACE Y	SURFACE X	PT NO	SURFACE Y	SURFACE X	PT NO	SURFACE Y	SURFACE X
1	-2.2725E+00	-2.2725E+00	2	-2.1851E+00	-2.1851E+00	3	-2.1851E+00	-2.1851E+00
2	-2.1851E+00	-2.1851E+00	4	-2.1851E+00	-2.1851E+00	5	-2.1851E+00	-2.1851E+00
3	-2.1851E+00	-2.1851E+00	6	-2.1851E+00	-2.1851E+00	7	-2.1851E+00	-2.1851E+00
4	-2.1851E+00	-2.1851E+00	8	-2.1851E+00	-2.1851E+00	9	-2.1851E+00	-2.1851E+00
5	-2.1851E+00	-2.1851E+00	10	-2.1851E+00	-2.1851E+00	11	-2.1851E+00	-2.1851E+00
6	-2.1851E+00	-2.1851E+00	12	-2.1851E+00	-2.1851E+00	13	-2.1851E+00	-2.1851E+00
7	-2.1851E+00	-2.1851E+00	14	-2.1851E+00	-2.1851E+00	15	-2.1851E+00	-2.1851E+00
8	-2.1851E+00	-2.1851E+00	16	-2.1851E+00	-2.1851E+00	17	-2.1851E+00	-2.1851E+00
9	-2.1851E+00	-2.1851E+00	18	-2.1851E+00	-2.1851E+00	19	-2.1851E+00	-2.1851E+00
10	-2.1851E+00	-2.1851E+00	20	-2.1851E+00	-2.1851E+00	21	-2.1851E+00	-2.1851E+00
11	-2.1851E+00	-2.1851E+00	22	-2.1851E+00	-2.1851E+00	23	-2.1851E+00	-2.1851E+00
12	-2.1851E+00	-2.1851E+00	24	-2.1851E+00	-2.1851E+00	25	-2.1851E+00	-2.1851E+00
13	-2.1851E+00	-2.1851E+00	26	-2.1851E+00	-2.1851E+00	27	-2.1851E+00	-2.1851E+00
14	-2.1851E+00	-2.1851E+00	28	-2.1851E+00	-2.1851E+00	29	-2.1851E+00	-2.1851E+00
15	-2.1851E+00	-2.1851E+00	30	-2.1851E+00	-2.1851E+00	31	-2.1851E+00	-2.1851E+00
16	-2.1851E+00	-2.1851E+00	32	-2.1851E+00	-2.1851E+00	33	-2.1851E+00	-2.1851E+00
17	-2.1851E+00	-2.1851E+00	34	-2.1851E+00	-2.1851E+00	35	-2.1851E+00	-2.1851E+00
18	-2.1851E+00	-2.1851E+00	36	-2.1851E+00	-2.1851E+00	37	-2.1851E+00	-2.1851E+00
19	-2.1851E+00	-2.1851E+00	38	-2.1851E+00	-2.1851E+00	39	-2.1851E+00	-2.1851E+00
20	-2.1851E+00	-2.1851E+00	40	-2.1851E+00	-2.1851E+00	41	-2.1851E+00	-2.1851E+00
21	-2.1851E+00	-2.1851E+00	42	-2.1851E+00	-2.1851E+00	43	-2.1851E+00	-2.1851E+00
22	-2.1851E+00	-2.1851E+00	44	-2.1851E+00	-2.1851E+00	45	-2.1851E+00	-2.1851E+00
23	-2.1851E+00	-2.1851E+00	46	-2.1851E+00	-2.1851E+00	47	-2.1851E+00	-2.1851E+00
24	-2.1851E+00	-2.1851E+00	48	-2.1851E+00	-2.1851E+00	49	-2.1851E+00	-2.1851E+00
25	-2.1851E+00	-2.1851E+00	50	-2.1851E+00	-2.1851E+00	51	-2.1851E+00	-2.1851E+00
26	-2.1851E+00	-2.1851E+00	52	-2.1851E+00	-2.1851E+00	53	-2.1851E+00	-2.1851E+00
27	-2.1851E+00	-2.1851E+00	54	-2.1851E+00	-2.1851E+00	55	-2.1851E+00	-2.1851E+00
28	-2.1851E+00	-2.1851E+00	56	-2.1851E+00	-2.1851E+00			
29	-2.1851E+00	-2.1851E+00						
30	-2.1851E+00	-2.1851E+00						
31	-2.1851E+00	-2.1851E+00						
32	-2.1851E+00	-2.1851E+00						
33	-2.1851E+00	-2.1851E+00						
34	-2.1851E+00	-2.1851E+00						
35	-2.1851E+00	-2.1851E+00						
36	-2.1851E+00	-2.1851E+00						
37	-2.1851E+00	-2.1851E+00						
38	-2.1851E+00	-2.1851E+00						
39	-2.1851E+00	-2.1851E+00						
40	-2.1851E+00	-2.1851E+00						
41	-2.1851E+00	-2.1851E+00						
42	-2.1851E+00	-2.1851E+00						
43	-2.1851E+00	-2.1851E+00						
44	-2.1851E+00	-2.1851E+00						
45	-2.1851E+00	-2.1851E+00						
46	-2.1851E+00	-2.1851E+00						
47	-2.1851E+00	-2.1851E+00						
48	-2.1851E+00	-2.1851E+00						
49	-2.1851E+00	-2.1851E+00						
50	-2.1851E+00	-2.1851E+00						
51	-2.1851E+00	-2.1851E+00						
52	-2.1851E+00	-2.1851E+00						
53	-2.1851E+00	-2.1851E+00						
54	-2.1851E+00	-2.1851E+00						
55	-2.1851E+00	-2.1851E+00						

POINTS DESCRIBING LANDING EDGE RADIUS

POINT NO.	X	Y
1	-2.2745E+00	-7.8986E-01
2	-2.2745E+00	-7.9178E-01
3	-2.2745E+00	-7.9151E-01
4	-2.2745E+00	-7.9214E-01
5	-2.2745E+00	-7.9274E-01
6	-2.2745E+00	-7.9343E-01
7	-2.2745E+00	-7.9413E-01
8	-2.2745E+00	-7.9483E-01
9	-2.2745E+00	-7.9553E-01
10	-2.2745E+00	-7.9623E-01
11	-2.2745E+00	-7.9693E-01
12	-2.2745E+00	-7.9763E-01
13	-2.2745E+00	-7.9833E-01
14	-2.2745E+00	-7.9903E-01
15	-2.2745E+00	-7.9973E-01
16	-2.2745E+00	-8.0043E-01
17	-2.2745E+00	-8.0113E-01
18	-2.2745E+00	-8.0183E-01
19	-2.2745E+00	-8.0253E-01
20	-2.2745E+00	-8.0323E-01
21	-2.2745E+00	-8.0393E-01
22	-2.2745E+00	-8.0463E-01
23	-2.2745E+00	-8.0533E-01
24	-2.2745E+00	-8.0603E-01
25	-2.2745E+00	-8.0673E-01
26	-2.2745E+00	-8.0743E-01
27	-2.2745E+00	-8.0813E-01
28	-2.2745E+00	-8.0883E-01
29	-2.2745E+00	-8.0953E-01
30	-2.2745E+00	-8.1023E-01
31	-2.2745E+00	-8.1093E-01

CARTESIAN COORDINATES ON CYCLOIDAL RADIUS

POINT NO	X1	Y1	X2	Y2
1	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
2	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
3	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
4	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
5	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
6	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
7	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
8	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
9	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
10	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
11	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
12	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
13	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
14	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
15	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
16	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01
17	4.9497E+00	-7.7617E-01	-2.1442E+00	-7.9015E-01

POINT NO	Z1	V1	V1	Z2	V2
18	7.77070000	-1.54304000	-1.78880000	-1.54304000	-2.04117000
19	7.77640000	-1.54030000	-1.78880000	-1.46710000	-2.74130000
20	7.04140000	-1.47144000	-1.43170000	-1.46710000	-2.62770000
21	7.02710000	-1.47144000	-1.43170000	-1.46710000	-2.47950000
22	7.02710000	-1.47144000	-1.43170000	-1.46710000	-2.33570000
23	7.02710000	-1.47144000	-1.43170000	-1.46710000	-2.19500000
24	7.02710000	-1.47144000	-1.43170000	-1.46710000	-2.05000000
25	7.02710000	-1.47144000	-1.43170000	-1.46710000	-1.90500000
26	7.02710000	-1.47144000	-1.43170000	-1.46710000	-1.76000000
27	7.02710000	-1.47144000	-1.43170000	-1.46710000	-1.61500000
28	7.02710000	-1.47144000	-1.43170000	-1.46710000	-1.47000000
29	7.02710000	-1.47144000	-1.43170000	-1.46710000	-1.32500000
30	7.02710000	-1.47144000	-1.43170000	-1.46710000	-1.18000000
31	7.02710000	-1.47144000	-1.43170000	-1.46710000	-1.03500000
32	7.02710000	-1.47144000	-1.43170000	-1.46710000	-0.89000000
33	7.02710000	-1.47144000	-1.43170000	-1.46710000	-0.74500000
34	7.02710000	-1.47144000	-1.43170000	-1.46710000	-0.60000000
35	7.02710000	-1.47144000	-1.43170000	-1.46710000	-0.45500000
36	7.02710000	-1.47144000	-1.43170000	-1.46710000	-0.31000000
37	7.02710000	-1.47144000	-1.43170000	-1.46710000	-0.16500000
38	7.02710000	-1.47144000	-1.43170000	-1.46710000	-0.02000000
39	7.02710000	-1.47144000	-1.43170000	-1.46710000	0.12500000
40	7.02710000	-1.47144000	-1.43170000	-1.46710000	0.27000000
41	7.02710000	-1.47144000	-1.43170000	-1.46710000	0.41500000
42	7.02710000	-1.47144000	-1.43170000	-1.46710000	0.56000000
43	7.02710000	-1.47144000	-1.43170000	-1.46710000	0.70500000
44	7.02710000	-1.47144000	-1.43170000	-1.46710000	0.85000000
45	7.02710000	-1.47144000	-1.43170000	-1.46710000	0.99500000
46	7.02710000	-1.47144000	-1.43170000	-1.46710000	1.14000000
47	7.02710000	-1.47144000	-1.43170000	-1.46710000	1.28500000
48	7.02710000	-1.47144000	-1.43170000	-1.46710000	1.43000000
49	7.02710000	-1.47144000	-1.43170000	-1.46710000	1.57500000
50	7.02710000	-1.47144000	-1.43170000	-1.46710000	1.72000000
51	7.02710000	-1.47144000	-1.43170000	-1.46710000	1.86500000
52	7.02710000	-1.47144000	-1.43170000	-1.46710000	2.01000000
53	7.02710000	-1.47144000	-1.43170000	-1.46710000	2.15500000
54	7.02710000	-1.47144000	-1.43170000	-1.46710000	2.30000000
55	7.02710000	-1.47144000	-1.43170000	-1.46710000	2.44500000
56	7.02710000	-1.47144000	-1.43170000	-1.46710000	2.59000000
57	7.02710000	-1.47144000	-1.43170000	-1.46710000	2.73500000

POINT NO	Z1	V1	V1	Z2	V2
1	6.04100000	-7.14412000	-7.91550000	-7.91550000	-1.12600000
2	6.04100000	-7.14412000	-7.91550000	-7.91550000	-1.27100000
3	6.04100000	-7.14412000	-7.91550000	-7.91550000	-1.41600000
4	6.04100000	-7.14412000	-7.91550000	-7.91550000	-1.56100000
5	6.04100000	-7.14412000	-7.91550000	-7.91550000	-1.70600000
6	6.04100000	-7.14412000	-7.91550000	-7.91550000	-1.85100000
7	6.04100000	-7.14412000	-7.91550000	-7.91550000	-1.99600000
8	6.04100000	-7.14412000	-7.91550000	-7.91550000	-2.14100000
9	6.04100000	-7.14412000	-7.91550000	-7.91550000	-2.28600000
10	6.04100000	-7.14412000	-7.91550000	-7.91550000	-2.43100000
11	6.04100000	-7.14412000	-7.91550000	-7.91550000	-2.57600000
12	6.04100000	-7.14412000	-7.91550000	-7.91550000	-2.72100000
13	6.04100000	-7.14412000	-7.91550000	-7.91550000	-2.86600000
14	6.04100000	-7.14412000	-7.91550000	-7.91550000	-3.01100000
15	6.04100000	-7.14412000	-7.91550000	-7.91550000	-3.15600000

POINT NO	ZSEMT	YSEMT	YSEMT
16	A.019919+00	-2.210019+00	-7.075775-01
17	A.019923+00	-2.210116+00	-7.017895-01
18	A.019924+00	-2.210277+00	-7.000125-01
19	A.019927+00	-2.210377+00	-7.800015-01
20	A.019928+00	-2.210529+00	-7.899165-01
21	A.019931+00	-2.210612+00	-7.878155-01
22	A.019935+00	-2.210675+00	-7.866665-01
23	A.019937+00	-2.210775+00	-7.854775-01
24	A.019938+00	-2.210915+00	-7.807635-01
25	A.019941+00	-2.210961+00	-7.819135-01
26	A.019943+00	-2.210991+00	-7.819135-01
27	A.020115+00	-2.210455+00	-7.906045-01
28	A.020135+00	-2.210485+00	-7.796225-01
29	A.020351+00	-2.210315+00	-7.772825-01
30	A.020722+00	-2.210395+00	-7.771955-01
31	A.020931+00	-2.210239+00	-7.761745-01

4. DISCUSSION OF EXAMPLE B

This example uses only the aerodynamic section of the program, and demonstrates the turbulent mixing calculation and the blade wake transfer calculation. The machine for which the computation is made is the so-called NACA Five-Stage Compressor that is described in References 2 and 3. A conventional multi-stage analysis calculation is set up, with a computing station at each blade edge (that is, there are two stations between each blade row). For each of the ten blade rows in the machine, fixed relative outlet flow angle and (two-dimensional) loss coefficient distributions are specified. The distributions are ones that describe well the performance of the blade rows at an operating point in the vicinity of the machine's design point, except that the loss coefficients do not reflect any variation in blade section performance with blade section location. In practical terms, this means that no additional rotor tip losses are incorporated. The wake transfer analysis was developed to account for migration of boundary layer material and is therefore applicable to the diffusion loss component of the relative total pressure loss coefficients. However, the subject compressor operates transonically in all stages at design speed, and so the rotor loss coefficients in the input data generally include a shock loss component in addition to the diffusion loss component. The input data item that controls the wake transfer rate, CONTR, is set to 1.0. The value is probably lower than it should be, and this compensates to some extent for the fact that (for the rotors) the whole loss coefficient is being manipulated instead of just the diffusion loss portion thereof. The input eddy viscosity, CONMX, is set to $2.0 \text{ ft}^2/\text{sec}$ which is higher than the probable correct value.

A listing of the input data cards is shown in the next sub section, and the corresponding output from the program follows. The program has computed the results with difficulty, although just a few more iterations are apparently required for total convergence. With a final IVFAIL of 5 and final IFFAIL of 0, the result may be taken to be converged for most practical purposes. The following points should be noted when examining the results. When wake transfer calculations are made, the loss coefficients shown in the results differ from those in the input. When turbulent mixing calculations are made, the loss coefficients shown in the results differ from those in the input and efficiencies computed for streamlines may take on apparently impossible values because both of these parameters are computed from conditions on "streamlines".

It is of some interest to examine the effects of the wake transfer and mixing calculations upon the computed compressor performance, and shown below are some performance parameters for the four possible calculation modes involving (or not involving) wake transfer and mixing. The final station (outlet) total temperature difference between casing and hub streamlines is shown as indicative of the effects of the various calculations

upon the distributions of properties of the flow. All computations were made with identical data, except that the input data items NTRANS and NMIX were varied as shown.

NTRANS	NMIX	Total Pressure Ratio	Isentropic Efficiency	(T case - T h _{in}) at outlet, deg.
0	0	5.188	.8313	40.9
0	1	5.264	.8341	3.9
1	0	4.524	.8073	259.4
1	1	4.512	.8086	194.8

It is apparent that the wake transfer calculation can drastically effect the machine overall performance and the distribution of properties of the flow. Also, the mixing calculation had considerably less effect on the overall performance, but did modify the distributions appreciably. It should be recalled that the calculations were somewhat simplified in that the relative outlet angles and base (two-dimensional) loss coefficients were fixed throughout.

Some final notes are given, as follows.

- 1) Correlation of empirical and computed results is needed to establish appropriate values for the wake transfer rate constant, CONTR, and the eddy inviscosity, CONMX.
- 2) In order to correctly apply the wake transfer calculation to transonic blade rows the computer program should be modified so that shock and diffusion loss coefficient components may be separately manipulated.
- 3) If it is desired to use the wake transfer calculation when computing stations are located within blade rows, the program will need modification. Probably the only change would be to replace I-1 with I + NLI (I) (separately computed) wherever it occurs in the call statement starting on card \$AR\$. 225.
- 4) Both the wake transfer and mixing calculations substantially increase computation time. For a fixed number of iterations, each of these options taken separately increases computation time by a factor of approximately three, and taken together by a factor of approximately six. In the case of the wake transfer calculation option, taken above or with the mixing calculation option, this is further compounded by the fact that it increases the number of iterations required for solution by a factor of two or three.

5. INPUT DATA CARD LISTING FOR EXAMPLE B

NACA 5-STAGE COMPRESSOR		FIVE CASCADE 2-D PERFORMANCE	
0	1	0	1
NACA 5-STAGE COMPRESSOR MIXING AND WAKE TRANSFERS CALCULATED			
0.0	25	1	1
13			
0.0			
0.0			
1.0		2.0	
46.5		1.0	
2			
-9.0		4.35	
-9.0		10.0	
2			
-3.0		4.35	
-3.0		10.0	
2			
0.0		5.0	
0.416		1.0	
2			
2.5		5.52	
2.085		10.0	
2			
3.25		5.7	
3.25		10.0	
2			
5.25		5.02	
5.25		10.0	
2			
5.425		5.0	
5.75		10.0	
2			
8.964		5.62	
8.539		10.0	
2			
9.625		5.75	
9.625		10.0	
2			
11.625		7.0	
11.625		10.0	
2			

12.750	7.20
13.157	10.0
2	
15.268	7.45
14.063	10.0
2	
16.0	7.50
2	10.0
17.0	7.60
2	10.0
19.126	7.70
19.349	10.0
2	
21.375	7.90
21.150	10.0
2	
22.125	7.90
22.125	10.0
2	
24.125	8.1
24.125	10.0
2	
25.25	9.15
25.300	10.0
2	
27.240	9.20
27.114	10.0
2	
28.0	9.25
29.0	10.0
2	
30.0	9.25
2	10.0
33.0	9.25
33.0	10.0
1	
	14.0

5:9.7

0	0	5	0	0	5	1	-1	-1
12605.1								
5.53				-0.201				.891
0.0								
6.543				-19.619				.18722
0.6								
7.6457				-21.021				.12186
0.7								
8.8046				-43.668				.15226
0.0								
13.3				-50.414				.17483
0.0								

0	5	0	0	5	1	-1	-1
---	---	---	---	---	---	----	----

0.0				7.568				.17268
6.02								
0.0								
6.89				3.419				.17579
0.0								
7.854				.052				.13465
0.0								
0.0								
8.939				-1.405				.12622
0.0								
10.3				-2.0				.12688
0.0								

0	5	0	0	5	1	-1	-1
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12605.1								
6.62				-0.668				.16722
0.0								
7.329				-21.282				.16791
0.0								
8.147				-22.124				.19180
0.0								
9.044				-43.554				.12631
0.7								
10.0				-47.420				.17585

0.0	1	0	0	5	1	-1	-1
0.0							
7.03				7.232			.742
0.0							
7.032				4.457			.810
0.0							
8.351				3.025			.5704
0.0							
9.144				1.610			.4542
0.0							
10.0				-0.130			.3785
0.0							
0							
5	0	0	0	5	1	-1	-1
12535.1							
7.45				-20.757			.9629
0.0							
7.955				-27.556			.5757
0.0							
8.571				-25.59.			.2177
0.0							
9.254				-42.677			.11717
0.0							
10.0				-48.951			.22561
0.0							
0							
5	0	0	0	5	1	-1	-1
0.0							
7.59				5.501			.78337
0.0							
8.137				3.040			.19533
0.0							
8.595				2.232			.07514
0.0							
9.312				.280			.6185
0.0							
10.0				-1.712			.4476
0.0							

[illegible]

3	0	7	5	2	-1	-1
0.0						
8.25		4.94				.15978
0.0						
8.5947		2.270				.16023
0.0						
8.99375		1.934				.16480
0.0						
9.4688		.537				.16151
0.0						
10.0		-0.907				.13818
0.0						
0.0						
0.0						
0.031						
0.034						
0.076						
0.060						
0.090						
0.085						
0.191						
0.174						
0.235						
0.196						
0.329						
0.304						
0.336						
0.299						
0.515						
0.473						
0.480						
0.448						
0.736						
0.717						
0.803						
0.821						

6. OUTPUT DATA FOR EXAMPLE B

PROGRAM UC13-0 - COMPRESSOR DESIGN - CONTROL SECTION
.....

TITLE = NACA 5-STAGE COMPRESSOR FIXED CASCADE 2-D PERFORMANCE
NUMBER OF ANALYTIC HEADLINE ULAH-00MS = 0
THERE WILL BE AN ENTRY TO THE AERODYNAMIC SECTION
NUMBER OF ARBITRARY HEADLINE ULAH-00MS = 0

STATION 4	SPECIFIED BY 2 POINTS
XSTN	ACTN
2.5000	5.5000
2.0000	10.0000
STATION 5	SPECIFIED BY 2 POINTS
XSTN	ACTN
3.2000	5.7000
3.2000	10.0000
STATION 6	SPECIFIED BY 2 POINTS
XSTN	ACTN
5.2500	6.3200
7.2500	10.0000
STATION 7	SPECIFIED BY 2 POINTS
XSTN	ACTN
6.4200	10.0000
6.7600	10.0000
STATION 8	SPECIFIED BY 2 POINTS
XSTN	ACTN
8.4400	9.0000
9.6100	10.0000
STATION 9	SPECIFIED BY 2 POINTS
XSTN	ACTN
9.6200	6.7500
9.6200	10.0000
STATION 10	SPECIFIED BY 2 POINTS
XSTN	ACTN
11.6200	7.0000
11.6200	10.0000
STATION 11	SPECIFIED BY 2 POINTS
XSTN	ACTN
12.7300	7.2200
13.0900	10.0000
STATION 12	SPECIFIED BY 2 POINTS
XSTN	ACTN
15.2600	7.4500
16.0000	10.0000
STATION 13	SPECIFIED BY 2 POINTS
XSTN	ACTN
16.0000	7.6300
16.0000	10.0000
STATION 14	SPECIFIED BY 2 POINTS
XSTN	ACTN
18.6000	6.6800
19.0000	10.0000

STATION 15 SPECIFIED BY 2 POINTS
 XSTN RSTN
 19.1200 7.7990
 19.3490 10.0000

STATION 16 SPECIFIED BY 2 POINTS
 XSTN RSTN
 21.3250 7.0300
 21.1500 10.0000

STATION 17 SPECIFIED BY 2 POINTS
 XSTN RSTN
 22.1220 7.0000
 22.1250 10.0000

STATION 18 SPECIFIED BY 2 POINTS
 XSTN RSTN
 24.1200 8.1000
 24.1250 10.0000

STATION 19 SPECIFIED BY 2 POINTS
 XSTN RSTN
 25.3500 8.1000
 25.3450 10.0000

STATION 20 SPECIFIED BY 2 POINTS
 XSTN RSTN
 27.2000 8.2300
 27.1100 10.0000

STATION 21 SPECIFIED BY 2 POINTS
 XSTN RSTN
 28.0000 8.2500
 28.0100 10.0000

STATION 22 SPECIFIED BY 2 POINTS
 XSTN RSTN
 30.0200 8.5500
 30.0000 10.0000

STATION 23 SPECIFIED BY 2 POINTS
 XSTN RSTN
 33.0000 8.2500
 33.0000 10.0000

STATION CALCULATION DATA
 STATION 1 NDATA= 1 INTER=0 NOINTER=0 MMACH=0
 DATAC TOTAL PRESSURE TOTAL TEMPERATURE WHIRL ANGLE
 -0.0000 14.7000 518.700 -0.000

STATION 2 NDATA= 0 INTER=0 NOINTER=0 MMACH=0
 DATAC TOTAL PRESSURE TOTAL TEMPERATURE WHIRL ANGLE
 -0.0000 14.7000 518.700 -0.000

STATION 3 NDATA= 0 INTER=0 NOINTER=0 MMACH=0
 DATAC TOTAL PRESSURE TOTAL TEMPERATURE WHIRL ANGLE
 -0.0000 14.7000 518.700 -0.000

[illegible]

STREAM LINE
 INLET THROUGH STATION 8
 PRESSURE EFFICIENCY OF H1
 STATION 7 THROUGH STATION 8
 PRESSURE EFFICIENCY OF H1
 MEAN VALUES TO
 INLET TO STA. 8 STA. 7 TO STA. 8
 MEAN VALUES TO
 INLET TO STA. 8 STA. 7 TO STA. 8

STREAM LINE
 INLET THROUGH STATION 8
 PRESSURE EFFICIENCY OF H1
 STATION 7 THROUGH STATION 8
 PRESSURE EFFICIENCY OF H1
 MEAN VALUES TO
 INLET TO STA. 8 STA. 7 TO STA. 8
 MEAN VALUES TO
 INLET TO STA. 8 STA. 7 TO STA. 8

STATION 9 FLOW-SECTION

STREAM LINE
 INLET THROUGH STATION 8
 PRESSURE EFFICIENCY OF H1
 STATION 7 THROUGH STATION 8
 PRESSURE EFFICIENCY OF H1
 MEAN VALUES TO
 INLET TO STA. 8 STA. 7 TO STA. 8
 MEAN VALUES TO
 INLET TO STA. 8 STA. 7 TO STA. 8

STREAM LINE
 INLET THROUGH STATION 8
 PRESSURE EFFICIENCY OF H1
 STATION 7 THROUGH STATION 8
 PRESSURE EFFICIENCY OF H1
 MEAN VALUES TO
 INLET TO STA. 8 STA. 7 TO STA. 8
 MEAN VALUES TO
 INLET TO STA. 8 STA. 7 TO STA. 8

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NOTES ON THE SUBMISSION OF MANUSCRIPTS TO THE JOURNAL OF POLYMER SCIENCE PART A-1

[illegible]

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STATION' 19 IS WITHIN OR AT THE TRAILING EDGE OF A BLADE ROTATING AT 0.0 RPM NUMBER OF BLADES IN ROW = 10
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[illegible]

STEELM
LINE
INLET THROUGH STATION 13
PRESSURE IS NOT COPIED
STATION 17 THROUGH STATION 18
PRESSURE IS NOT COPIED
MEAN VALUES
PRESSURE
INLET TO STA. 18
STA. 17 TO STA. 18

[illegible]

[illegible]

STREAM -LINE	MACH NUMBER	TOTAL PRESSURE STATIC	TOTAL TEMPERATURE STATIC	WEIGHT SPECIFIC	TOTAL ENTHALPY STATIC	ENTROPY	FLOW ANGLE	(PHI+GAMMA)
1	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
2	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
3	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
4	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
5	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
6	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
7	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
8	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
9	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
10	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
11	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000

STREAM -LINE	BLADE COUNT	RELATIVE VELOCITY	RELATIVE MACH NO.	RELATIVE FLOW ANGLE	DEVIATION ANGLE	BLADE ANGLE	LANE PRESSURE OFF	DIFFUSION FACTOR	DELTA ON D
1	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
2	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
3	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
4	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
5	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
6	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
7	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
8	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
9	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
10	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
11	0.0	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000

STREAM -LINE	INLET PRESSURE	INLET TEMPERATURE	INLET WEIGHT SPECIFIC	INLET ENTHALPY STATIC	INLET ENTROPY	INLET FLOW ANGLE	INLET (PHI+GAMMA)
1	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
2	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
3	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
4	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
5	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
6	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
7	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
8	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
9	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
10	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
11	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000

STREAM -LINE	STATION 21 RADIUS	STATION 21 FLOW ANGLE	STATION 21 PRESSURE	STATION 21 TEMPERATURE	STATION 21 WEIGHT SPECIFIC	STATION 21 ENTHALPY STATIC	STATION 21 ENTROPY	STATION 21 FLOW ANGLE	STATION 21 (PHI+GAMMA)
1	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
2	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
3	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
4	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
5	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
6	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
7	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
8	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
9	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
10	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
11	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000

[illegible]

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